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JC960 U.S. PTO

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09/723733Please type a plus sign (+) inside this box → ☐Approved for use through 09/30/2000. OMB 0651-0032
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UTILITY PATENT APPLICATION TRANSMITTAL (Only for new nonprovisional applications under 37 C.F.R. § 1.53(b))	Attorney Docket No.	1300-009
	First Inventor or Application Identifier	HORTON
	Title	UV Disinfection for Wastewater Treatment
	Express Mail Label No.	EF068536335US

APPLICATION ELEMENTS See MPEP chapter 600 concerning utility patent application contents.	ADDRESS TO: Assistant Commissioner for Patents Box Patent Application Washington, DC 20231	
1. <input checked="" type="checkbox"/> * Fee Transmittal Form (e.g., PTO/SB/17) (Submit an original and a duplicate for fee processing)	5. <input type="checkbox"/> Microfiche Computer Program (Appendix)	
2. <input checked="" type="checkbox"/> Specification [Total Pages 65] (preferred arrangement set forth below) <ul style="list-style-type: none">- Descriptive title of the Invention- Cross References to Related Applications- Statement Regarding Fed sponsored R & D- Reference to Microfiche Appendix- Background of the Invention- Brief Summary of the Invention- Brief Description of the Drawings (if filed)- Detailed Description- Claim(s)- Abstract of the Disclosure	6. Nucleotide and/or Amino Acid Sequence Submission (if applicable, all necessary) <ul style="list-style-type: none">a. <input type="checkbox"/> Computer Readable Copyb. <input type="checkbox"/> Paper Copy (identical to computer copy)c. <input type="checkbox"/> Statement verifying identity of above copies	
3. <input checked="" type="checkbox"/> Drawing(s) (35 U.S.C. 113) [Total Sheets 7]	ACCOMPANYING APPLICATION PARTS 7. <input type="checkbox"/> Assignment Papers (cover sheet & document(s)) 8. <input type="checkbox"/> 37 C.F.R. § 3.73(b) Statement <input type="checkbox"/> Power of Attorney (when there is an assignee) 9. <input type="checkbox"/> English Translation Document (if applicable) 10. <input checked="" type="checkbox"/> Information Disclosure Statement (IDS)/PTO-1449 <input type="checkbox"/> Copies of IDS Citations 11. <input type="checkbox"/> Preliminary Amendment 12. <input checked="" type="checkbox"/> Return Receipt Postcard (MPEP 503) (Should be specifically itemized) 13. <input checked="" type="checkbox"/> * Small Entity Statement(s) <input type="checkbox"/> Statement filed in prior application, Status still proper and desired (PTO/SB/09-12) 14. <input type="checkbox"/> Certified Copy of Priority Document(s) (if foreign priority is claimed) 15. <input type="checkbox"/> Other: _____	
4. Oath or Declaration [Total Pages 2] <ul style="list-style-type: none">a. <input checked="" type="checkbox"/> Newly executed (original or copy)b. <input type="checkbox"/> Copy from a prior application (37 C.F.R. § 1.63(d)) (for continuation/divisional with Box 16 completed)<ul style="list-style-type: none">i. <input type="checkbox"/> DELETION OF INVENTOR(S) Signed statement attached deleting inventor(s) named in the prior application, see 37 C.F.R. §§ 1.63(d)(2) and 1.33(b).		
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16. If a CONTINUING APPLICATION , check appropriate box, and supply the requisite information below and in a preliminary amendment. <input type="checkbox"/> Continuation <input type="checkbox"/> Divisional <input checked="" type="checkbox"/> Continuation-in-part (CIP) of prior application No: 09, 630245 Prior application information: Examiner _____ Group / Art Unit: _____ For CONTINUATION or DIVISIONAL APPS only: The entire disclosure of the prior application, from which an oath or declaration is supplied under Box 4b, is considered a part of the disclosure of the accompanying continuation or divisional application and is hereby incorporated by reference. The incorporation <u>can only</u> be relied upon when a portion has been inadvertently omitted from the submitted application parts.		

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Name (Print/Type)	JiNan Glasgow	Registration No. (Attorney/Agent)	42585
Signature		Date	11/28/2000

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See 37 C.F.R. §§ 1.27 and 1.28.

TOTAL AMOUNT OF PAYMENT (\$)**845**

Complete if Known

Application Number
Filing Date 11/28/2000
First Named Inventor HORTON
Examiner Name
Group / Art Unit
Attorney Docket No. 1300-009

METHOD OF PAYMENT (check one)

1. ☐ The Commissioner is hereby authorized to charge indicated fees and credit any overpayments to:

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☐ Charge Any Additional Fee Required
Under 37 CFR §§ 1.16 and 1.17

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FEE CALCULATION

1. BASIC FILING FEE

Large Entity Code	Large Entity Fee (\$)	Small Entity Code	Small Entity Fee (\$)	Fee Description	Fee Paid
101	690	201	345	Utility filing fee	355
106	310	206	155	Design filing fee	
107	480	207	240	Plant filing fee	
108	690	208	345	Reissue filing fee	
114	150	214	75	Provisional filing fee	

SUBTOTAL (1) (\$)**355**

2. EXTRA CLAIM FEES

Total Claims	Extra Claims	Fee from below	Fee Paid
30	20** = 50	9	450
4	3** = 1	40	40
Multiple Dependent			

**or number previously paid, if greater; For Reissues, see below

Large Entity Code	Large Entity Fee (\$)	Small Entity Code	Small Entity Fee (\$)	Fee Description
103	18	203	9	Claims in excess of 20
102	78	202	39	Independent claims in excess of 3
104	260	204	130	Multiple dependent claim, if not paid
109	78	209	39	** Reissue independent claims over original patent
110	18	210	9	** Reissue claims in excess of 20 and over original patent

SUBTOTAL (2) (\$)**490**

FEE CALCULATION (continued)

3. ADDITIONAL FEES

Large Entity Code	Large Entity Fee (\$)	Small Entity Code	Small Entity Fee (\$)	Fee Description	Fee Paid
105	130	205	65	Surcharge - late filing fee or oath	
127	50	227	25	Surcharge - late provisional filing fee or cover sheet	
139	130	139	130	Non-English specification	
147	2,520	147	2,520	For filing a request for reexamination	
112	920*	112	920*	Requesting publication of SIR prior to Examiner action	
113	1,840*	113	1,840*	Requesting publication of SIR after Examiner action	
115	110	215	55	Extension for reply within first month	
116	380	216	190	Extension for reply within second month	
117	870	217	435	Extension for reply within third month	
118	1,360	218	680	Extension for reply within fourth month	
128	1,850	228	925	Extension for reply within fifth month	
119	300	219	150	Notice of Appeal	
120	300	220	150	Filing a brief in support of an appeal	
121	260	221	130	Request for oral hearing	
138	1,510	138	1,510	Petition to institute a public use proceeding	
140	110	240	55	Petition to revive - unavoidable	
141	1,210	241	605	Petition to revive - unintentional	
142	1,210	242	605	Utility issue fee (or reissue)	
143	430	243	215	Design issue fee	
144	580	244	290	Plant issue fee	
122	130	122	130	Petitions to the Commissioner	
123	50	123	50	Petitions related to provisional applications	
126	240	126	240	Submission of Information Disclosure Stmt	
581	40	581	40	Recording each patent assignment per property (times number of properties)	
146	690	246	345	Filing a submission after final rejection (37 CFR § 1.129(a))	
149	690	249	345	For each additional invention to be examined (37 CFR § 1.129(b))	

Other fee (specify) _____

Other fee (specify) _____

* Reduced by Basic Filing Fee Paid

SUBTOTAL (3) (\$)

SUBMITTED BY

Name (Print/Type)	JiNan Glasgow	Registration No. (Attorney/Agent)	23485	Telephone	919-664-8222
Signature		Date			

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STATEMENT CLAIMING SMALL ENTITY STATUS
(37 CFR 1.9(f) & 1.27(c))--SMALL BUSINESS CONCERN

Docket Number (Optional)
1300-009

Applicant, Patentee, or Identifier: HORTON
Application or Patent No.: _____
Filed or Issued: 11/28/2000
Title: UV DISINFECTION FOR WASTEWATER

I hereby state that I am

- ☐ the owner of the small business concern identified below:
☒ an official of the small business concern empowered to act on behalf of the concern identified below:

NAME OF SMALL BUSINESS CONCERN REMOTELIGHT.COM, INC.

ADDRESS OF SMALL BUSINESS CONCERN RALEIGH, NORTH CAROLINA

I hereby state that the above identified small business concern qualifies as a small business concern as defined in 13 CFR Part 121 for purposes of paying reduced fees to the United States Patent and Trademark Office. Questions related to size standards for a small business concern may be directed to: Small Business Administration, Size Standards Staff, 409 Third Street, SW, Washington, DC 20416.

I hereby state that rights under contract or law have been conveyed to and remain with the small business concern identified above with regard to the invention described in:

- ☒ the specification filed herewith with title as listed above.
☐ the application identified above.
☐ the patent identified above.

If the rights held by the above identified small business concern are not exclusive, each individual, concern, or organization having rights in the invention must file separate statements as to their status as small entities, and no rights to the invention are held by any person, other than the inventor, who would not qualify as an independent inventor under 37 CFR 1.9(c) if that person made the invention, or by any concern which would not qualify as a small business concern under 37 CFR 1.9(d), or a nonprofit organization under 37 CFR 1.9(e).

Each person, concern, or organization having any rights in the invention is listed below:

- ☐ no such person, concern, or organization exists.
☒ each such person, concern, or organization is listed below.

Separate statements are required from each named person, concern or organization having rights to the invention stating their status as small entities. (37 CFR 1.27)

I acknowledge the duty to file, in this application or patent, notification of any change in status resulting in loss of entitlement to small entity status prior to paying, or at the time of paying, the earliest of the issue fee or any maintenance fee due after the date on which status as a small entity is no longer appropriate. (37 CFR 1.28(b))

NAME OF PERSON SIGNING Isaac B. Horton, III

TITLE OF PERSON IF OTHER THAN OWNER CEO

ADDRESS OF PERSON SIGNING Raleigh, North Carolina

SIGNATURE [Signature] DATE 11/28/2000

UNITED STATES APPLICATION

FOR

GRANT OF LETTERS PATENT

BY ISAAC B. HORTON, III
of Raleigh, North Carolina, USA

FOR

UV DISINFECTION FOR WASTEWATER

GLASGOW LAW FIRM
Intellectual Property Law
PO Box 28539
116 N. West St. Suite 270
Raleigh, NC 27611-8539

Atty Docket No. 1300-009

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1 **ULTRAVIOLET WASTEWATER DISINFECTION SYSTEM AND METHOD**

2 CROSS-REFERENCE TO RELATED APPLICATIONS

3 This non-provisional utility patent application claims the benefit of one or more
4 prior filed co-pending non-provisional applications; a reference to each such prior
5 application is identified as the relationship of the applications and application number
6 (series code/serial number): The present application is a Continuation-In-Part of
7 application 09/630245, which is incorporated herein by reference in its entirety.

8 Background of the Invention

9 (1) Field of the Invention

10 The present invention relates generally to a system and method for ultraviolet
11 disinfection and, more particularly, to a system and method for ultraviolet disinfection of
12 waste-containing fluids.

13 (2) Description of the Prior Art

14 *Mechanism of Action*

15 It is well known in the art to use ultraviolet light (UV) for the disinfection
16 treatment of water. Ultraviolet light, at the germicidal wavelength of 253.7 nanometers,
17 alters the genetic (DNA) material in cells so that bacteria, viruses, molds, algae and other
18 microorganisms can no longer reproduce. The microorganisms are considered dead, and
19 the risk of disease from them is eliminated. As the water flows past the UV lamps in UV
20 disinfection systems, the microorganisms are exposed to a lethal dose of UV energy. UV
21 dose is measured as the product of UV light intensity times the exposure time within the
22 UV lamp array. Microbiologists have determined the effective dose of UV energy to be
23 approximately about 34,000 microwatt- seconds/cm² needed to destroy pathogens as well

1 as indicator organisms found in wastewater. Typical prior art disinfection systems and
2 devices emit UV light at approximately 254 nm, which penetrates the outer cell
3 membrane of microorganisms, passes through the cell body, reaches the DNA and alters
4 the genetic material of the microorganism, destroying it without chemicals by rendering it
5 unable to reproduce.

6 Ultraviolet light is classified into three wavelength ranges: UV-C, from about 200
7 nanometers (nm) to about 280 nm; UV-B, from about 280 nm to about 315 nm; and UV-
8 A, from about 315 nm to about 400 nm. Generally, UV light, and in particular, UV-C
9 light is "germicidal," i.e., it deactivates the DNA of bacteria, viruses and other pathogens
10 and thus destroys their ability to multiply and cause disease, effectively resulting in
11 sterilization of the microorganisms. Specifically, UV "C" light causes damage to the
12 nucleic acid of microorganisms by forming covalent bonds between certain adjacent
13 bases in the DNA. The formation of these bonds prevents the DNA from being
14 "unzipped" for replication, and the organism is unable to produce molecules essential for
15 life process, nor is it able to reproduce. In fact, when an organism is unable to produce
16 these essential molecules or is unable to replicate, it dies. UV light with a wavelength of
17 approximately between about 250 to about 260 nm provides the highest germicidal
18 effectiveness. While susceptibility to UV light varies, exposure to UV energy for about
19 20 milliwatt-seconds/cm² is adequate to deactivate 99 percent of the pathogens.

20

1

2 *Prior Art*

3 Ultraviolet light has a proven track record of killing bacteria and viruses found in
4 municipal wastewater. In addition, environmental concerns over the use of chemical
5 disinfectants, coupled with improvements in ultraviolet-lighting technology, have led to
6 the development of UV systems that treat spent metalworking fluids in the industrialized
7 world; disinfect drinking water in developing countries; and clean aquaculture water,
8 ballast water, and hospital air everywhere. Typically, chlorine gas or liquid is injected by
9 a high-speed inductor directly into wastewater to kill bacteria before the water is
10 discharged. According to industry experts, the main advantage of using UV instead of
11 standard disinfection techniques is elimination of the transport and use of chlorine
12 possible with the UV light-based system.

13 Unfortunately, evidence is mounting that organic chemical byproducts of
14 chemical disinfection, especially byproduct of chlorination such as dioxane, are
15 carcinogens and/or toxins for humans. Therefore, chemical disinfection is not a viable
16 alternative when chemical purity of the fluid is desired and/or required. Additionally, in
17 spite of this toxicological evidence, the EPA has recently been forced to relax restrictions
18 on certain known carcinogenic chlorination by-product, such as chloroform.
19 Additionally, other chemicals, such as the nitrate ion, have been shown to negatively
20 influence the development of children.

21 In light of the emerging data concerning the toxicity of organic and inorganic
22 chemicals and the relaxation of water purity regulations, reducing the discharge into the
23 environment of these compounds is of growing concern. However, removal of these

1 compounds requires the use of extremely expensive methods, such as filtration through
2 activated charcoal or similar. Thus, there exists a need for a system that can easily
3 remove or eliminate organic and inorganic compounds from wastewater.

4 Used properly, ultraviolet light effectively destroys bacteria, viruses and other
5 microorganisms in water and wastewater, without using chemicals. By doing away with
6 chemical treatment, many other problems are also eliminated. There is no longer any
7 need to worry about operator safety or the requirement for buildings for storage and
8 handling of dangerous solutions and gases. Costly liability insurance premiums are
9 significantly reduced. Testing of effluent for chlorine residual is no longer necessary, and
10 toxicity problems associated with chlorine use are eliminated. Another factor leading
11 municipalities to reconsider chlorination is its increased cost due to the national Uniform
12 Fire Code adopted in 1993, which specifies expensive requirements for double
13 containment of stored chlorine and chemical scrubbers in case of leaks.

14 Prior art applications of UV light used for disinfection of water include private
15 drinking water supplies, municipal drinking water treatment plants, industrial product and
16 process waters, and commercial applications, and wastewater treatment in primary,
17 secondary, and tertiary treatment process for industrial, commercial and municipal
18 wastewater treatment applications.

19 While UV purification is well suited for many residential, commercial, industrial
20 and municipal water and wastewater treatment applications, considerations of the water
21 quality and about the desired or required effluent purity impact the system design and
22 performance. Prior art UV disinfectant systems work best when the water temperature is

1 between about 35 and about 110 degrees Fahrenheit, since extreme cold or heat will
2 interfere with the UV system performance.

3 The UV light source used in prior art are typically low pressure mercury lamps,
4 which can effectively clean water of dangerous and illness-causing viruses and bacteria,
5 including intestinal protozoa such as Cryptosporidium, Giardia, and E.coli, provided that
6 the proper number and configuration of lamps are included in the system. All known
7 prior art systems calculate, design and configure the proper number and arrangement or
8 positioning of lamps as set forth and described by formulas developed and published by
9 Dr. George Tchobanoglous, presently of University of California at Davis.

10 Dr. George Tchobanoglous, professor emeritus of civil and environmental
11 engineering at the University of California, Davis and former chairperson on a committee
12 of academic, industrial, and environmental consultants who drafted guidelines on UV
13 disinfection for California in 1994, is perhaps the leading authority on UV water
14 disinfectant systems and methods used in the prior art. His formulas for predicting the
15 minimum required number of UV lamps and configuration of same are based on a key
16 component of positioning the UV lamps within the water to be treated, and more
17 particularly, requiring a lamp centerline-to-centerline distance of not more than three (3)
18 inches to ensure effective disinfectant UV dosage for any influent system and flow rate;
19 these formulas referred to as "point source summation".

20 Traditional low-pressure UV systems found in the prior art are used for low flow
21 water disinfection or smaller projects with air and surface applications. The low pressure
22 UV lamp treats between 10 and 180 gallons per minute of fluid using up to 12 lamps at a
23 time. As flows increase or higher UV doses are required, the multiple low-pressure lamp

1 concept becomes complex and cumbersome. The medium pressure UV lamp offers a
2 solution to maintain simplicity and cost effectiveness in meeting the higher flow and
3 higher dose challenge. A single medium pressure UV lamp can treat up to 2,300 gallons
4 per minute of fluid. Notably, the UV disinfection systems and methods used by prior art
5 consistently involve and teach the use of low pressure UV lamp and equipment for water,
6 air and surface disinfection applications. These prior art systems require treatment
7 chambers, usually constructed of stainless steel. The prior art air systems also use low-
8 pressure UV lamps and treat air in storage tanks.

9 Where the prior art uses a medium pressure UV lamp, typically single lamp units
10 are used, possibly capable of treating 10 to 2,300 gallons per minute of fluid. In these
11 cases, prior art requires special enhanced medium pressure UV lamps, with these
12 applications restricted for use treating high and low temperature fluids that are
13 unachievable with low-pressure lamps. Even with such configurations, the use of
14 immersion-positioned UV lamps in an effective chamber design still requires system
15 downtime to change the UV lamp. Special enhanced UV lamp design is required to
16 achieve the highest performance in TOC reduction, ozone removal and chlorine
17 destruction.

18 Problems exist for prior art systems where factors are present that inhibit UV light
19 from penetrating the water. Turbidity, which is the state of water when it is cloudy from
20 having sediment stirred up, interferes with the transmission of UV energy and decreases
21 the disinfection efficiency of the UV light disinfection system. In cases where the water
22 has high iron or manganese content, is clouded and/or has organic impurities, it is usually
23 necessary to pre-treat the water before it enters the UV disinfection stage because

1 deposits on the quartz-encased UV lamps, which are immersed in the water to be treated,
2 interfere with the UV light transmission, thereby reducing the UV dose and rendering the
3 system ineffective. Prior art typically employs UV purification in conjunction with
4 carbon filtration, reverse osmosis and with certain chemicals to reduce fouling between
5 cleanings of the quartz sleeves that surround the UV lamps.

6 Typically, prior art devices and systems for disinfecting water via ultraviolet light
7 exposure commonly employ standard ultraviolet light sources or lamps encased in quartz
8 sleeves and suspended in the water being treated. Benefits of using ultraviolet light for
9 disinfecting water, particularly waste water treatment, include the following: no
10 chemicals, like chlorine, are needed to ensure effective water disinfection provided that
11 the proper number of lamps are used and properly positioned for a given influent and
12 flow rate; since no chemicals are required in the disinfection process, no storage and/or
13 handling of toxic chemicals is required; no heating or cooling is required to ensure
14 disinfection; no storage tanks or ponds are necessary because the water can be treated as
15 it flows through the system; no water is wasted in the process; no change in pH, chemical
16 or resistivity of the water being treated; approximately at least 99.99% of all waterborne
17 bacteria and viruses are killed via UV light exposure for disinfection; thereby providing
18 increased safety of using the system and effectiveness of same.

19 As set forth in the foregoing, prior art UV water treatment systems disinfect and
20 remove microorganisms and other substances from untreated, contaminated water sources
21 and produce clean, safe drinking water. The core technology employed in WaterHealth
22 International's system is includes a patented, non-submerged UV light. This technology
23 is claimed by WHI to be a recent and tested innovation developed at the Lawrence

1 Berkeley National Laboratory, a premier, internationally respected laboratory of the U.S.
2 Department of Energy managed by the University of California. This prior art system
3 delivers a UV dose of up to 120 mJ/cm², which is more than three times the NSF
4 International requirement of 38 mJ/cm² and exceeds World Health Organization and
5 EPA water quality standards and effectively treats bacteria, viruses and *Cryptosporidium*
6 in drinking water. In addition, recent research conducted at two different laboratories
7 indicates that UV doses of 10 mJ/cm² or less produce 4-log reductions in *Giardia*. Based
8 on this research, UV dosage of up to 120 mJ/cm² greatly exceeds the dosage required for
9 inactivation of *Giardia*. Additional components included in WaterHealth International's
10 systems effectively treat specific problems such as turbidity, silt, tastes, odors and various
11 chemicals. Significantly, WHI's systems are not intended to treat raw sewage or
12 wastewater.

13 Among applications for UV disinfection systems for water include wastewater
14 treatment and surface treatment. By way of example and explanation, disinfection of
15 municipal wastewater using UV light avoids problems associated with storage, transport
16 and use of chemicals and associated regulation for them. UV disinfection is safe, cost
17 effective and applicable to tertiary treated effluent as well as secondary, primary, and
18 combined sewer overflows (CSO) and storm water. Ultraviolet light can help improve
19 shelf life of products and allow processors to reduce chemical additives in wash water
20 without sacrificing high levels of disinfection. UV light provides non-chemical microbial
21 control for captive water loops without altering the taste, color or odor of the food.
22 Environmentally safe UV disinfection is one of the few water treatment methods

1 unburdened by regulatory restrictions, consumer/environmental group concerns or high
2 operation costs.

3 By way of comparison between prior art UV disinfection systems and traditional
4 chlorine-based disinfection, the commercially available Trojan UV system can disinfect
5 more consistently and effectively than is possible with current chlorination procedures,
6 with significantly less cost per gallon. The UV treatment takes approximately 6-10
7 seconds in a flow-through channel, while chlorine requires 15-20 minutes treatment time
8 in a contact tank. According to Trojan literature, UV disinfection can greatly reduce
9 capital and operating costs. With UV treatment, it is possible to eliminate the need for
10 large contact tanks designed to hold peak flows. Space requirements are reduced and no
11 buildings are needed since the entire process and related commercially available
12 equipment are designed to operate outdoors.

13 However, cleaning and maintenance of the quartz sleeves, which are necessary
14 and essential to protect the UV lamp or light source used in nearly all prior art systems,
15 can become a time-consuming duty, especially when working with multi-lamp low
16 pressure systems. During operation while the UV lamps and quartz sleeves are
17 suspending in the water to be treated, minerals and contaminants in the water deposit
18 onto the quartz sleeves, thereby causing fouling on the sleeve surface. This fouling
19 reduces the effectiveness of the UV lamps because the fouling interferes with the UV
20 light transmission into the water. To save time and prevent quartz sleeve fouling a
21 cleaning mechanism can be supplied for either manual or automatic operation, like using
22 wiper glides over the sleeves to remove deposits, which may block the light emitted from
23 the UV lamp. This provides improved performance and reduces maintenance time, but

1 only where the water quality is low. In every case, the UV lamps encased in quartz
2 sleeves must be removed for cleaning on at least a monthly basis, depending on specifics
3 of a given system and its influent and flow rates. The cleaning requires the system to be
4 shut down temporarily or diverted to other UV lamps, so system shut down decreases
5 capacity and/or increases operating costs. Furthermore, the quartz sleeve-encased lamps
6 are extremely heavy, requiring the use of a crane to raise them out of the water flow
7 stream for cleaning. Cranes and crane time are expensive, thereby increasing overall
8 system costs. Only one company, WaterHealth, Inc., might in any way suggest the use of
9 non-submerged lamps for UV systems but these are limited expressly in advertising
10 literature as applicable only and exclusively in applications that do not require high
11 purification, e.g., previously purified drinking water but not wastewater treatment.

12 These prior art systems do not employ optical components nor reflective materials
13 or photocatalytic materials in the holding tank and reaction vessels.

14 Thus, there remains a need for a UV disinfection system for treating waste-
15 containing fluids having reduced maintenance time and costs, increased flow rates for a
16 given disinfection level, and overall lower equipment, installation, and system costs.

17 Additionally, there remains a need for water purification system that can remove or
18 degrade organic compounds and other chemical contaminants in fluids with reduced
19 maintenance and expense.

20 Summary of the Invention

21 The present invention is directed to a UV disinfection and chemical reduction
22 system and method for treating waste-containing fluids, particularly wastewater, whereby
23 the UV light or other activating wavelengths can effectuate catalytic reduction of water-

1 borne chemicals and the UV light source requires less maintenance and cost than prior art
2 systems and devices while providing at least the same disinfection level for a given
3 influent and flow rate thereof.

4 One object of the present invention is to provide a UV disinfection system for
5 treating waste-containing fluids configured and arranged to function effectively with at
6 least one UV light source or lamp that is not submerged in the fluid to be disinfected.
7 The UV light source is positioned outside the fluid to be disinfected via exposure to at
8 least one UV dose zone wherein UV light is projected into the zone.

9 Another object of the present invention includes presentation of the UV light
10 source presented in at least two primary configurations: a vertical riser configuration and
11 a planar or horizontal configuration. In the vertical riser configuration the UV light
12 source is positioned above the waste-containing fluid to be treated and projecting a UV
13 dose zone downward toward and into the waste-containing fluid to be treated, with the
14 waste-containing fluid moving upward toward the UV light source. Alternatively, the
15 UV light source may be presented in a planar or horizontal design, wherein the UV light
16 source is positioned above the waste-containing fluid to be treated and projecting a UV
17 dose zone downward toward and into the waste-containing fluid to be treated, with the
18 waste-containing fluid moving in a direction substantially perpendicular to the UV dose
19 zone.

20 Still another object of the present invention is to provide a UV dose zone
21 including at least one zone, more preferably four zones, wherein one zone includes an
22 interface zone positioned between the UV light source and the fluid to be treated and
23 another zone includes a reaction zone positioned within the fluid. The reaction zone may

1 be formed by an interface plate that incorporates catalytic properties to enhance desired
2 reactions.

3 The present invention is further directed to a method for treating waste-containing
4 fluids by disinfecting those waste-containing fluids using UV light projected by at least
5 one UV light source producing at least one dose zone, the UV light source being
6 positioned outside the waste-containing fluid.

7 Accordingly, one aspect of the present invention is to provide a system and
8 method for disinfecting waste-containing fluid including at least one UV light source
9 positioned outside the waste-containing fluid to be treated with the at least one UV light
10 source producing at least one UV dose zone for disinfecting the waste-containing fluid.

11 Another aspect of the present invention is to provide a system and method for
12 disinfecting and purifying fluid including at least one UV light source positioned outside
13 the fluid to be treated with the at least one UV light source producing four UV dose zones
14 for disinfecting the fluid, with one zone provided at an interface zone, and one zone
15 provided at a reaction zone positioned between the UV light source and the fluid to be
16 treated. The reaction zone may be formed by an interface plate that incorporates catalytic
17 properties to enhance desired reactions

18 Still another aspect of the present invention is to provide a system and method for
19 disinfecting waste-containing fluid including at least one UV light source positioned
20 outside the waste-containing fluid to be treated with the at least one UV light source
21 producing at least one UV dose zone for disinfecting the waste-containing fluid, wherein
22 the at least one UV light source is a medium-to-high intensity UV light source or spectral
23 calibration lamp.

1 These and other aspects of the present invention will become apparent to those
2 skilled in the art after a reading of the following description of the preferred embodiment
3 when considered with the drawings.

4 Brief Description of the Drawings

5 Figure 1 is an illustration of **PRIOR ART** in a side view.

6 Figure 2 is an illustration of a side view of a UV disinfection system constructed
7 according to the present invention in a vertical riser configuration.

8 Figure 3 is an illustration of an exploded side view of the embodiment shown in Fig. 2.

9 Figure 4 shows an illustration of a UV disinfection system of an alternative embodiment
10 of the present invention.

11 Figure 5 is an illustration of an exploded side view of the embodiment shown in Fig. 4.

12 Figure 6 is an illustration of the UV dose zones generated in a vertical riser configuration.

13 Figure 7 is an illustration of the UV dose zones generated in an alternative embodiment
14 of the present invention.

15 Detailed Description of the Preferred Embodiments

16 In the following description, like reference characters designate like or
17 corresponding parts throughout the several views. Also in the following description, it is
18 to be understood that such terms as "forward," "rearward," "front," "back," "right,"
19 "left," "upwardly," "downwardly," and the like are words of convenience and are not to
20 be construed as limiting terms.

21 Referring now to the drawings in general, the illustrations are for the purpose of
22 describing a preferred embodiment of the invention and are not intended to limit the
23 invention thereto. Figure 1 shows a prior art system for ultraviolet (UV) disinfection of a

1 waste-containing fluid wherein the UV light source PA16 is submerged in the waste-
2 containing fluid. Untreated influent PA12 enters the system flowing past the submerged
3 light source and exits the output as treated disinfected effluent PA14. By contrast to prior
4 art, the present invention is directed to an ultraviolet (UV) disinfection system and
5 method for treating fluids including a configuration and design to function effectively
6 with at least one UV light source or lamp that is not submerged in the fluid.

7 Advantageously, the non-submerged configuration of the present invention
8 prevents the problems associated with breakage of the lamp and/or lamp housing and
9 fouling of the lamp housing. Additionally, the non-submerged configuration of the
10 present invention prevents the problems associated with extreme temperatures in the
11 fluid. Fluorescent lamps, including UV lamps, lose a significant amount of output at low
12 temperatures. Thus, a non-submerged system, which separates the lamp from the fluid
13 to be treated, allows for the temperature of the lamp to be maintained at more optimal
14 temperature, without necessitating cooling or heating the fluid as well. Thus, this system
15 more efficiently disinfects extreme environments, such as freezers, coolers, hot water
16 heaters, and the like.

17 *Vertical Riser Configuration (VRC)*

18 The UV light source may be presented in a vertical riser configuration according
19 to a preferred embodiment of the present invention, as shown generally at 100 in Figure
20 2, wherein the fluid exits a reservoir or holding container 110 via a pipe or outlet 120 into
21 the vertical riser configuration (VRC) 200 and passes therethrough prior to discharge
22 from the pipe or outlet 140 for consumption or end use. Furthermore, the VRC, as shown
23 generally at 200 in Figure 3, includes at least one UV light source 310. This UV light

source 310 is part of a lamp assembly, as shown generally at 300 in Figure 5. The lamp assembly 300 is composed of a housing 320 that encases the UV light source 310, UV light rays 330, at least one optical component 340, and UV light ray output 350 that exits the housing. Referring to Figure 3, the UV light ray output 350 exits the housing above the fluid 210 to be treated, this fluid entering the VRC from the outlet pipe 120 of the holding container or reservoir 110 and being forced upward through the interior pipe 220 of the VRC 200 toward the UV light ray output 350 that is projected downward toward the fluid surface 230 and into the fluid 210 to be treated, once again with the fluid moving upward toward the UV light source 310. At least one interface plate 240 may be fitted to the top of the interior pipe 220, thus increasing the exposure time of the fluid 210 to the UV light ray output 350. The at least one interface plate 240 contains a hole or holes 250 that allows fluid rising upward through the interior pipe 220 to exit at the top of the pipe. The fluid then traverses across the superior surface 260 of the interface plate 240 to the plate edge 270, where it then descends into the exterior chamber 280 of the VRC. The fluid is prevented from returning into the interior pipe 220 by a base plate 290 that solidly connects the exterior of the interior pipe 220 with the interior of the outer pipe 295. The fluid then exits the VRC 200 through the pipe or outlet 140. The UV light rays 330 may be projected downward from a UV light source or a lamp system 310 that includes optical components. These optical components may include, but are not limited to, reflectors, shutters, lenses, splitters, focalizers, mirrors, rigid and flexible light guides, homogenizer or mixing rods, manifolds and other couplers, filters, gratings, diffractors, color wheels, and the like. These optical components are internal to the lamp system and are positioned between the UV light source or lamp 310 and the UV ray light output 350

1 of the lamp assembly 300, thereby focusing, directing, and controlling the light ray output
2 350 that irradiates the fluid 210 and that sterilizes any microorganisms that exist in the
3 fluid 210. The UV light ray output 350 irradiates and may also be transmitted through
4 the fluid 210. UV light ray output 350 that is transmitted through the fluid and strikes the
5 reflective interior surfaces (not shown) of the VRC components is reflected back into the
6 fluid where it may strike microorganism. The reflection of the UV light ray output 350
7 back into the fluid by the reflective interior surfaces of the VRC components enhances
8 the killing capacity of the VRC system 200.

9 Additionally, the interface plate may possess catalytic properties such that certain
10 reactions are catalyzed in the vicinity of the interface plate. For example, TiO_2 may be
11 incorporated into the interface plate that is made of glass or other appropriate material.
12 When such a plate is irradiated with UV light, fatty acids and other organic chemicals are
13 chemically reduced, resulting in degradation to smaller volatile products such as
14 methane, ethane, etc. Additionally, nitrate ion is reduced to elemental nitrogen in such a
15 system. Thus, the incorporation of TiO_2 into the interface plate with subsequent UV
16 irradiation reduces the levels of two potential human toxins – organic chemicals and
17 nitrate ion. The interface plate may also perform mechanical or other physical functions.
18 For example, the plate may grind and/or sift particles contained within the fluid. The
19 plate may also provide cooling, heat, steam, or gas(es) to the reaction zone to enhance
20 desired reactions or inhibit undesired reactions. Heat, steam, or other gases may also be
21 added in order to increase the vapor zone. In general, the interface plate can be used to
22 facilitate surface reactions and/or surface/air reactions.

1 Advantageously, the disinfected, purified water that exits the total system from
2 the VRC device is completely free from microorganisms without requiring the addition of
3 chemicals or other additives that would increase the total dissolved solids in the water.

4 *Reservoir Configuration*

5 Alternatively or in combination with the VRC system, a non-VRC configuration
6 is advantageously constructed and configured to provide UV disinfection from a non-
7 submerged UV light source for a reservoir, holding container, or other non-flowing water
8 storage, however temporary the water dwell time may be. Preferably, the fluid is pre-
9 treated water that has already been disinfected and purified, possibly with low total
10 dissolved solids therein. This pretreatment may have occurred in a VRC system that
11 incorporates a catalytic plate to reduce organic and inorganic contaminants in the water,
12 in addition to disinfecting the water. As illustrated in Figures 4 & 5, the present
13 invention, generally referenced 400, is a non-riser configuration (NRC) that includes at
14 least one UV light source 310. This UV light source 310 is part of a lamp assembly, as
15 shown generally at 300 in Figure 5. The lamp assembly 300 is composed of a housing
16 320 that encases the UV light source 310, UV light rays 330, at least one optical
17 component 340, and UV light ray output 350 that exits the housing. Referring to Figure
18 4, the UV light ray output 350 exits the housing 320 above the fluid 212 to be treated, this
19 fluid being held in a holding container or reservoir 112 and not being forced toward UV
20 light ray output 350 that is projected downward toward the fluid surface 232 and into the
21 fluid to be treated 212, once again with the fluid 212 not being forced toward the UV
22 light source 310. The UV light ray output 350 may be projected downward from a UV
23 light source or a lamp system 300 that includes optical components as previously

1 described. These optical components may include, but are not limited to, reflectors,
2 shutters, lenses, splitters, focalizers, mirrors, rigid and flexible light guides, homogenizer
3 or mixing rods, manifolds and other couplers, filters, gratings, diffractors, color wheels,
4 and the like. These optical components are internal to the lamp system and are positioned
5 between the UV light source or lamp 310 and the UV ray light output 350 of the lamp
6 system 300, thereby focusing, directing, and controlling the light ray output 350 that
7 irradiates the fluid 212 and that sterilizes any microorganisms that exist in the fluid 212.
8 The UV light ray output 350 irradiates and may also be transmitted through the fluid 212.
9 UV light ray output 350 that is transmitted through the fluid and strikes the reflective
10 interior surface of the holding tank or container 112 is reflected back into the fluid where
11 it may strike microorganism. The reflection of the UV light ray output 350 back into the
12 fluid by the reflective interior surface of the holding tank or container 112 enhances the
13 killing capacity of the NRC system 400.

14 *Planar Configuration*

15 Alternatively to the vertical and reservoir configurations, the UV light source may
16 be presented in a planar or horizontal design (not shown), wherein the UV light source is
17 positioned within a UV light source system, including optical components, above the
18 waste-containing fluid to be treated and projecting a UV dose zone downward toward and
19 into the waste-containing fluid to be treated, with the waste-containing fluid moving from
20 the influent point in a direction substantially perpendicular to the UV light source toward
21 the effluent point.

22 A key factor in the design of a UV disinfection system and method according to
23 the present invention involves the integration of two main components, including the

1 non-submerged UV light source system and the hydraulic system. The light source
2 system includes a housing surrounding and supporting a UV light source or lamp having
3 at least one optical component positioned and arranged to direct the UV light rays toward
4 and through an output, thereby introducing UV light rays toward a waste-containing fluid
5 for disinfection of the fluid.

6 The hydraulic system includes a hydraulic tube and pumping system for forcing
7 the waste-containing fluid upward through the tube toward the light source(s). The present
8 invention includes the use of hydraulic systems that comprise a transporter or pumping
9 system, and at least one interface plate. The hydraulic system serves at least three
10 functions: it carries wastewater influent to an interface and provides flow to at least one
11 interface plate and discharges the treated influent water as effluent to rivers or streams.
12 The VRC system may include quick-connect lamps and housings with a monitoring and
13 indicator system that would indicate that a lamp had failed. Each riser may have an
14 individual, dedicated lamp and optical system with overlap between neighboring lamps to
15 eliminate dead zone. Each riser in the VRC system may also have a valve that shuts off
16 the riser in case of failure.

17 Advantageously, these systems have several UV dose zones established within
18 them. In the VRC system, as best shown in Figs. 3 and 5, the UV light source 310 is
19 positioned within a UV light source system 300, including optical components as
20 previously described, above the fluid to be treated and projecting a UV dose zone
21 downward toward and into the fluid to be treated, with the fluid moving from the influent
22 point 120, flowing vertically up the interior pipe 220 toward the UV light source 310, and
23 then exiting the interior pipe 220 through the interface plate 240. The at least one UV

1 light source is positioned above the fluid to be treated and projecting UV light ray output
2 350 downward toward and into the fluid to be treated, with the fluid moving upward
3 toward the UV light source. Several UV dose zones are established within the VRC
4 system, generally shown as 500 in Fig. 6. The first zone is the light source system exit
5 UV dose zone 510, which occurs at the light source system and air interface. Then next
6 zone is the air UV dose zone 520, which occurs just beneath the UV light source and just
7 above the water and the at least one interface plate 240. The next zone is the vapor zone
8 525, which occurs just above the water surface. The next zone is the interface plate UV
9 dose zone 530, which occurs at the intersection of the water and the at least one interface
10 plate 240. The at least one interface plate is used to provide a reaction zone for UV
11 disinfection of fluid flowing over the plate and to provide additional treatment means for
12 balancing pH, affecting effluent chemistry, providing a catalyst, and the like. For
13 example, TiO_2 may be incorporated into the interface plate to effect reduction of ions and
14 compounds. Specifically, TiO_2 is used to reduce nitrates and nitrites to elemental
15 nitrogen. Such a treatment is desirable, in that nitrates have been linked to developmental
16 defects in children. Additionally, TiO_2 incorporated in glass and irradiated with UV light
17 will degrade fatty acids and other organic compounds adjacent to exterior of the glass.
18 Thus, such a plate can be used to degrade organic contaminants found in water.
19 Additionally, UV light can catalyze a variety of reactions, and the use of UV light with
20 any one or combination of the plethora of available chemical catalyst generates numerous
21 possible catalytic combinations that are used to catalyze a myriad of desirable reactions.
22 The photocatalyst may include photo-activated semiconductors such as Titanium Oxide;
23 TiO_2 (photo activation wavelength; not more than 388 nm), Tungsten Oxide; WO_2

1 (photo activation wavelength; not more than 388 nm), Zinc Oxide; ZnO (photo activation
2 wavelength; not more than 388 nm), Zinc Sulfide; ZnS (photo activation wavelength; not
3 more than 344 nm) and Tin Oxide; SnO₂ (photo activation wavelength; not more than
4 326 nm). In addition to these catalysts, other catalysts, such as PtTiO₂, are known. TiO₂
5 may be preferably applied as the photocatalyst, considering that the activation power is
6 very high, the catalyst is long-lived with high durability, and safety for human
7 applications is certified, as TiO₂ has been used safely for a long time in cosmetic and
8 food applications. Additionally, the interface plate may be a biofilter, and contain
9 enzymes or bacteria that react with substrates contained in the fluid.

10 The last zone is the submerged UV dose zone 540, which creates a variable UV
11 dose zone that decreases in effectiveness at greater distances from the UV light source.

12 For the generally static non-riser configuration, the zones are different than those
13 described in the VRC system. In the generally static non-riser system, generally shown
14 as 600 in Fig. 7, the first zone is the light source system exit UV dose zone 610, which
15 occurs at the light source system and air interface. Then next zone is the air UV dose
16 zone 620, which occurs just beneath the UV light source and just above the water surface
17 230. The next zone is the vapor zone, which occurs just above the surface of the water.
18 The last zone is the submerged UV dose zone 640, which creates a variable UV dose
19 zone that decreases in effectiveness at greater distances from the UV light source.

20 For the planar configuration, the zones are different than the VRC and reservoir
21 configurations. Several UV dose zones are established within the system (not shown).
22 The first zone is the air UV dose zone that occurs just beneath the UV light source and
23 just above the water. The next zone is the air/water interface UV dose zone that occurs at

1 the air and water interface. The last zone is the submerged UV dose zone, which occurs
2 within the flowing water.

3 While generally regarding the UV light source and configuration thereof, the
4 preferred embodiment of the present invention includes at least one optical component
5 positioned between the UV light source and the UV light source system output point.
6 Advantageously, the use of optical components enables the system to maximize the
7 intensity, focus, and control of the UV light rays at the output for any given UV light
8 source or lamp. Also, optical components, including but not limited to reflectors,
9 shutters, lenses, splitters, mirrors, rigid and flexible light guides, homogenizer or mixing
10 rods, manifolds and other couplers, filters, color wheels, and the like, can be utilized in
11 combination to achieve the desired control and output, as set forth in U.S. patent numbers
12 6,027,237; 5,917,986; 5,911,020; 5,892,867; 5,862,277; 5,857,041; 5,832,151; 5,790,725;
13 5,790,723; 5,751,870; 5,708,737; 5,706,376; 5,682,448; 5,661,828; 5,559,911; D417,920
14 and co-pending applications 09/523,609 and 09/587,678 which are commonly owned by
15 the assignee of the present invention, and which are incorporated herein by reference in
16 their entirety. Additionally, optical component such as gratings, dichroic filters,
17 focalizers, gradient lenses, and off-axis reflectors may be used.

18 With regard to light guides, these may be fiberoptic lines composed of acrylic,
19 glass, liquid core, hollow core, core-sheath, or a combination.

20 With regard to lenses, several embodiments are envisioned. Imaging lenses, such
21 as a parabolic lens, and non-imaging lenses, such as gradient lenses, may be used. A
22 gradient lens collects light through a collecting opening and focuses it to an area smaller
23 than the area of the collecting opening. This concentration is accomplished by changing

1 the index of refraction of the lens along the axis of light transmission in a continuous or
2 semi-continuous fashion, such that the light is “funneled” to the focus area by refraction.
3 An example of gradient lens technology is the Gradium® Lens manufactured by Solaria
4 Corporation. Alternatively, a toroidal reflector, as described in United States Patent
5 5,836,667, is used. In this embodiment, a UV radiation source, such as an arc lamp, is
6 located at a point displaced from the optical axis of a concave toroidal reflecting surface.
7 The concave primary reflector focuses the radiation from the source at an off-axis image
8 point that is displaced from the optical axis. The use of a toroidal reflecting surface
9 enhances the collection efficiency into a small target, such as an optical fiber, relative to a
10 spherical reflecting surface by substantially reducing aberrations caused by the off-axis
11 geometry. A second concave reflector is placed opposite to the first reflector to enhance
12 further the total flux collected by a small target.

13 Additionally, more than one reflector may be used with a lamp. For example, dual
14 reflectors or three or more reflectors, as taught in US Patents 5,706,376 and 5,862,277,
15 may be incorporated into the preferred embodiment. These reflectors may also be
16 splitting reflectors and/or cascading reflectors.

17 In general, the transmissive optical components are UV transmissive and the
18 reflective optical components are UV reflective. Additionally, any of the optical
19 components, including the housing, may be made of acrylic or similar materials that
20 degrade over time when exposed to UV light. These components can be replaced when
21 their performance has deteriorated to an unacceptable level.

22 Notably, any number of lamps including low pressure, medium pressure, high
23 pressure, and ultra high-pressure lamps, which are made of various materials, e.g., most

1 commonly mercury (Hg), can be used with the system configuration according to the
2 present invention, depending upon the fluid or influent characteristics and flow rates
3 through the system. Furthermore, while high and ultra high pressure lamps have not been
4 used commercially to date by any prior art system, predominantly because of the low
5 energy efficiency associated with them and the lack of capacity for prior art design and
6 configuration formulas to include high pressure UV lamps, the present invention is
7 advantageously suited to accommodate medium to high to ultra high pressure lamps. In
8 particular, a preferred embodiment according to the present invention employs medium to
9 high-pressure UV lamps, more preferably high-pressure UV lamps. The present
10 invention is advantageously suited to accommodate medium to high to ultra high pressure
11 lamps, all of which can be metal, halogen, or a combination metal halide. Additionally,
12 spectral calibration lamps, electrodeless lamps, and the like can be used.

13 In particular, a preferred embodiment according to the present invention employs
14 a pencil-type spectral calibration lamp. These lamps are compact and offer narrow,
15 intense emissions. Their average intensity is constant and reproducible. They have a
16 longer life relative to other high wattage lamps. Hg (Ar) lamps of this type are generally
17 insensitive to temperature and require only a two-minute warm-up for the mercury vapor
18 to dominate the discharge, then 30 minutes for complete stabilization.

19 A Hg (Ar) UV lamp, which is presently commercially available and supplied by
20 ORIEL Instruments, is used in the preferred embodiment according to the present
21 invention. The ORIEL Hg(Ar) lamp, model 6035, emits UV radiation at 254 nm. When
22 operated at 15 mA using a DC power supply, this lamp emits 74 microwatt/cm² of 254
23 nm radiation at 25 cm from the source.

1 The system according to the present invention uses medium to high pressure UV
2 lamps configured and functioning above the fluid or water flow, not immersed in the
3 fluid flow as with all prior art systems designed for use in all water treatment
4 applications. With this system, the number of lamps necessary to treat a given influent
5 and flow rate can be reduced by perhaps a factor of ten, which is a major advantage in
6 practical application. Also, the lamps are not susceptible to fouling, since they are not
7 immersed in the fluid to be disinfected. Additionally, the design of the present invention
8 allows for a significant reduction in heat in the water. Furthermore, the maintenance and
9 servicing is greatly simplified. Also, in the vertical riser configuration according to one
10 preferred embodiment configuration, the reactor design, which would comprise a number
11 of cylindrical tubes oriented vertically, includes a hydraulic system having pumping
12 equipment and a significant amount of pumping power. Furthermore, the present
13 invention is an optical UV light source system for use in a waste-containing fluid
14 disinfection system. As such, traditional mathematical models used for determining
15 energy efficiencies for the present invention are inadequate and inapplicable. Thus, given
16 the use of optical components associated with the UV light source, the use of medium to
17 ultra high pressure UV lamps, and the introduction of at least one UV dose zone existing
18 outside the water to be treated, the present system presents a revolutionary approach for
19 designing, constructing, and operating a UV waste-containing fluid disinfection system
20 that is nowhere taught or suggested in the prior art or mathematical models for predicting
21 waste-containing fluid disinfection and flow rates thereof.

22 In one embodiment according to the present invention, the UV light source is a
23 Fusion RF UV lamp, which is presently commercially available and supplied by Fusion

1 UV Systems, Inc. The fusion lamp is a preferred lamp for a planar vertical riser system
 2 configuration, according to the present invention, to provide fast flow rates of the fluid
 3 treated within the system. This fusion lamp has a spectrum like a low-pressure lamp,
 4 having very strong UVB&C availability and output, but is a high power lamp having
 5 approximately 200W/cm. Significantly, as set forth in the foregoing, no prior art teaches
 6 or suggests the use of high pressure lamps, in fact, all standard formulas, including those
 7 developed by Dr. George Tchobanoglous, for system design and operation use low
 8 pressure lamps.

9 Surprisingly, the attached data supporting the novelty and non-obviousness of the
 10 present invention shows that the UVB&C efficacy for a high-pressure lamp is about 7-
 11 8%, compared to about 20-21% for a Germicidal lamp, and about 5% for a medium
 12 pressure lamp. Thus, one Fusion lamp would replace about 40 germicidal lamps or about
 13 20 medium pressure lamps by the following analysis:

14
$$\frac{[\# \text{ lamps of type x}]}{[\# \text{ lamps of type y}]} = \frac{[P/L(\text{type y})] \cdot [\text{Efficacy}(\text{type y})]}{[P/L(\text{type x})] \cdot [\text{Efficacy}(\text{type x})]}$$

15
$$\frac{[\# \text{ MPL}]}{[\# \text{ HPL}]} \sim \frac{[200 \cdot 8\%]}{[20 \cdot 5\%]} \sim 20$$

16
$$\frac{[\# \text{ LPL}]}{[\# \text{ HPL}]} \sim \frac{[200 \cdot 7\%]}{[2 \cdot 21\%]} \sim 40$$

17 Therefore, instead of having a facility with at least about 11,500 ea. 300 W MPLS as with
 18 prior art UV water disinfection systems, the present invention uses only a few hundred
 19 UV high-pressure lamps (HPL), depending on details of the design for a specific influent
 20 composition and flow rates desired for a given system. These results are surprising and
 21 not supported by prior art systems or the formulas used to design and configure them for
 22 effective operation. A variety of tubular lamp types may be used according to the present
 23

1 invention: Low Pressure (Power) germicidal Lamps (LPL), Medium Pressure (Power)
2 Lamps (MPL), and Ultra-High Power Lamps (UHPL), to be used with water of various
3 purity levels requiring differing dosing (Joules/liter) for disinfection, the surprising
4 results supporting the use of medium to high pressure UV lamps for the UV disinfection
5 system for water, according to the present invention, are established.

6 An additional advantage of high-power lamp systems is that extra-UV
7 wavelengths, when delivered at sufficient intensity, may destroy or otherwise inactivate
8 microorganisms as well. Several mechanisms of action are possible, but in general, the
9 high-dose light denatures cell components such as proteins, cell membranes, and the like
10 and inactivates the microorganism.

11 Additional considerations for a UV disinfectant system and method for treating
12 water are installation cost, and lamp life. The lamp life for the Fusion lamp is
13 approximately about 5000 hours, which is comparable to the low pressure lamps (LPL)
14 and comparable to the life of the medium pressure lamp (MPL). The installation cost of
15 the Fusion lamp is somewhat higher, but the maintenance and associated costs for
16 operation is lower, thereby providing an overall lower cost system when compared with
17 the prior art systems.

18 The system according to the present invention uses medium to high pressure UV
19 lamps configured and functioning above the fluid or water flow. With this system, the
20 number of lamps necessary to treat a given influent and flow rate can be reduced by
21 perhaps a factor of ten, which is a major advantage in practical application. Also, the
22 lamps are not susceptible to fouling, since they are not immersed in the waste-containing
23 fluid to be disinfected. Additionally, the design of the present invention allows for a

1 significant reduction in heat in the water. Furthermore, the maintenance and servicing is
2 greatly simplified. Also, in the vertical riser configuration according to one preferred
3 embodiment configuration, the reactor design, which would comprise a number of
4 cylindrical tubes oriented vertically, includes a hydraulic system having pumping
5 equipment and a significant amount of pumping power.

6 The present invention advantageously includes all of the above features, in
7 particular because the UV lamps are separated from the flow stream and include a fiber
8 optic delivery system, as well as using multi-kiloWatt lamps, like the Vortek Ultra-High
9 Power Discharge (UHPD) lamps or similar commercial equivalent. The power range for
10 these lamps is in the 10's of kiloWatts to MegaWatt range. There geometry is
11 cylindrical, like the medium power lamps, but they are roughly 1000 times more
12 powerful. Advantageously, this lamp provides a much simpler facility, wherein servicing
13 and maintenance are much easier and less frequently performed.

14 The flexibility of the UV waste-containing fluid disinfection system according to
15 the present invention makes it possible to use lamp configurations similar to prior art
16 systems for the overall geometry. However, the use of a much higher power lamp is
17 preferred, thereby reducing the water treatment facility complexity and costs. This novel
18 combination of higher pressure and power UV light sources in the present invention
19 creates surprising results, even where prior art system configurations, i.e., horizontal
20 flow-type configurations, are employed. Furthermore, the use of optical components
21 within the UV light source system to focus, control, and increase the output intensity of
22 the UV light rays introduced to the fluid to be disinfected increases the overall
23 effectiveness of the present invention, even where the retrofit geometry is employed.

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1 Thus, the present invention can be configured effectively either similarly to prior
2 art-like system or retrofit geometry, i.e., a configuration of lamps above a horizontal flow
3 stream while still surprisingly employing novel and non-obvious elements like UHPL and
4 HPL in combination therewith, or in a clear departure and in complete differentiation
5 from all prior art systems for all water treatment, having a configuration comprising the
6 vertical riser geometry as shown in Figure 2, including having at least one interface plate.
7 In the retrofit geometry or configuration, there is a turbulence-inducing foil immersed in
8 the flow stream below each lamp to assure that sufficient mixing occurs, thereby ensuring
9 exposure of all of the microorganisms within the waste-containing fluid to the UV dose
10 zone such that those microorganisms are sterilized. However, the use of the vertical riser
11 configuration creates even more surprising results in that a multiplicity of UV dose zones
12 are created as the fluid to be treated is forced via a hydraulic system toward the UV light
13 source system, including UV light source or lamp and optical component(s).

14 Two main types of lamps are embodied according to the present invention for use
15 therein as at least one light source for a given configuration. In particular, a tubular lamp
16 is generally approximately about 1000 mm long, and between about 30 to about 60 mm
17 diameter. A fusion lamp produces UV light output at about 250 mm and is
18 approximately about 8 mm diameter in the middle and approximately about 14 mm
19 diameter near the ends of the lamp. Alternatively, a high power, short arc (HP-SA) lamp
20 figure is preferred in other configurations. Significantly, alternative lamp embodiments,
21 including but not limited to alternative lamp design, power, and UV output efficiencies,
22 and reasonable equivalents thereof may be substituted for these lamps identified herein as

1 preferred embodiments without departing from the scope and teachings of the present
2 invention.

3 Characteristics of and advantages to the present invention include at least the
4 following: the use of Ultra High Power Lamps reduces complexity of illumination
5 system, the lamps are isolated from the flow stream eliminating the fouling problem,
6 since the UHPL, e.g., Vortek lamps, are immersed in their own flowing water cooling
7 jackets (purified water), much of the heat will be dissipated in the Vortek-type lamp
8 cooling system, probably eliminating the need for the heat-rejecting cold mirrors, since a
9 much smaller number of parts are used (most likely less than 1% of the parts), the
10 servicing costs are likely to be much lower. If the lamp life is longer for a given system
11 constructed according to the present invention, the servicing costs are reduced by a
12 similar factor as well.

13 The present invention allows a significantly simplified system, potentially
14 significantly lower operating costs, and the capacity to process large quantities of water
15 as well as relatively small quantities, as for home use. For a single-dwelling system, a
16 single vertical riser UV light source system, is constructed and configured to be attached
17 to the treated wastewater discharge. In this system, the UV light source is positioned
18 within a UV light source system, including optical components, above the fluid to be
19 treated and projecting a UV dose zone downward toward and into the fluid to be treated,
20 with the fluid moving from the influent point, flowing vertically toward the UV light
21 source, and then exits the effluent point. The at least one UV light source is positioned
22 above the fluid to be treated and projecting UV light rays downward toward and into the
23 fluid to be treated, with the fluid moving upward toward the UV light source. Several

1 UV dose zones are established within the system. The first zone is the light source
2 system exit UV dose zone, which occurs at the light source system and air interface.
3 Then next zone is the air UV dose zone which occurs just beneath the UV light source
4 and just above the water and the at least one interface plate. The next zone is the
5 interface plate UV dose zone, which occurs at the intersection of the water and the at
6 least one interface plate. The at least one interface plate is used to provide a surface zone
7 for UV disinfection above the fluid and to provide additional treatment means for
8 balancing pH, affecting effluent chemistry, providing a catalyst, and the like. The last
9 zone is the submerged UV dose zone, which creates a variable UV dose zone that
10 decreases in effectiveness at greater distances from the UV light source. Commercial-
11 scale applications for buildings or multi-family dwellings are constructed similarly, only
12 using a plurality of vertical riser units, as necessary for the water flow requirements of
13 that facility. Thus, a variety of features that have lead to a significant improvement to the
14 design of a UV disinfection system are shown, allowing simplified, lower cost facilities,
15 higher water processing rates, and an ultimately superior product.

16 An alternative embodiment of the present invention is connected to a fluid
17 reservoir. The first aspect of the reservoir system is a fluid reservoir. In this system, the
18 UV light source is positioned within a UV light source system, including optical
19 components, above the fluid stored in the reservoir and projecting a UV dose zone
20 downward toward and into the fluid to be pre-treated. This reservoir fluid could be
21 previously treated/purified or not. The at least one UV light source is positioned above
22 the fluid to be treated and projecting UV light rays downward toward and into the fluid to
23 be pre-treated. The light source system is provided in the reservoir system to prevent

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1 microorganism build-up in the reservoir. For completion of the system, a single vertical
2 riser UV light source system is constructed and configured to be attached to the reservoir
3 system. In this system, the UV light source is positioned within a UV light source
4 system, including optical components (not shown), above the fluid to be treated and
5 projecting a UV dose zone downward toward and into the fluid to be treated, with the
6 fluid moving from the influent point (reservoir effluent point), flowing vertically toward
7 the UV light source, and then exits the effluent point. The at least one UV light source is
8 positioned above the fluid to be treated and projecting UV light rays downward toward
9 and into the fluid to be treated, with the fluid moving upward toward the UV light source.
10 Several UV dose zones are established within the system. The first zone is the light
11 source system exit UV dose zone, which occurs at the light source system and air
12 interface. Then next zone is the air UV dose zone which occurs just beneath the UV light
13 source and just above the water and the at least one interface plate. The next zone is the
14 interface plate UV dose zone which occurs at the intersection of the water and the at least
15 one interface plate. The at least one interface plate is used to provide a surface zone for
16 UV disinfection above the fluid and to provide additional treatment means for balancing
17 pH, affecting effluent chemistry, providing a catalyst, and the like. The last zone is the
18 submerged UV dose zone, which creates a variable UV dose zone that decreases in
19 effectiveness at greater distances from the UV light source.

20 The foregoing described the general features of selected UV water disinfection
21 system applications, including wastewater treatment, other water purification, e.g.,
22 drinking water, and the like, for permanent or fixed-system installations and

1 configurations. However, the present invention is also useful for application in a portable
2 water disinfection system.

3 The following provides an alternate embodiment that includes selected desirable
4 features of the present invention. There are a number of very high power tubular lamps
5 that may be employed in another embodiment for UV light source system and hydraulic
6 system combinations. The medium pressure lamps could be used, albeit at a much higher
7 power level that was indicated for the commercially available Trojan Tech design
8 (300W). Medium pressure lamps are available in the multi-kiloWatt range. The high
9 power lamps, e.g., Vortek lamps, are a desirable source since they have strong UV
10 emission, and are available in the 100's of kW to MegaWatt range.

11 In one embodiment, the water flow is in a horizontal channel or direction, which
12 does not require all of the vertical riser components, like the interface plate and some
13 hydraulic components. However, optical components are desirably included in the planar
14 or horizontal (also referred to as retrofit) designs. The water turbulence could be achieved
15 by having horizontal "foils" (like those on the trailing edge of an airplane wing),
16 immersed in the flow channel. These foils would make a shallow turbulent region in the
17 flow channel allowing good exposure of the infected water past the lamps. In this simple
18 way, the function of the complex vertical riser would be achieved, with much fewer parts.

19 Thus the configuration includes a number of cylindrical or tubular light sources or
20 lamps oriented and arranged in a horizontally spaced-apart distance from each other in a
21 non-submerged configuration over a flowing fluid stream, with each lamp having a foil
22 positioned approximately directly under it to provide the turbulent flow mixing desired.

The fundamental physical parameters that control the design for these compact/short arc kinds of systems according to the present invention include: the lamp power per unit length [P]; the Cylindrical Riser flow tube Cross-section[A]; the dosing required [D] where $D = \text{Energy}/\text{volume}$, and the flow rate & dwell time. For the purposes of this analysis the cell widths are between about 10 cm and about 15 cm, the water penetration approximately about 10 cm. The dwell time depends on the effectiveness of the turbulent mixing, the influent characteristics, and type of contamination.

A cylindrical riser for cell of 10 to 15 cm diameter as being a practical size, thereby providing a disinfection dosage, $D = \text{Energy}/\text{volume} = E/V$ which varies from about 50 J/liter to perhaps 500 J/liter.

The three parameters T, P/A, and D control the possible/practical flow geometries. Since $P/V = E/V/T$ where P= input power, E= input energy, V = volume of water being processed & T = dwell time, then $P/[A*d] = D/T$

where $D = E/V$, the input energy/volume, or dosing

Then, $T = D*d/[P/A]$

$T = D(\text{J/liter}) * d(\text{cm}) * (1 \text{ liter}/1000\text{cm}^3) / [P/A(\text{W}/\text{cm}^2)]$.

Further, $P/A = P/[\pi * \text{dia} * \text{dia}/4] \sim 3000/[3.14 * 10 * 10/4] \sim 38 \text{ W}/\text{cm}^2$ for 3000W Hg, & a 4" diameter vertical riser configuration.

$P/A \sim 20000/[3.14 * 15 * 15/4] \sim 113 \text{ W}/\text{cm}^2$ for Xe & a 6" dia riser

TABLE 1

Dwell Time for Compact/Short-arc Mercury and Xenon Lamps					
		Dose (J/l)			
Lamp type V	Wattage	50	100	200	500
Mercury 40W/cm ²	40	0.013	0.025	0.050	0.125
Xenon 100W/cm ²	100	0.005	0.010	0.020	0.050

Surprisingly and significantly, these dwell times are much shorter than understood or set forth and commonly accepted and used within prior art. If the lamp power is reduced to 10%, and increase the cell diameter 2x, the results of Table 2 exist (SEE BELOW).

$P/A = P/[\pi \cdot \text{dia} \cdot \text{dia}/4] \sim 300/[3.14 \cdot 15 \cdot 15/4] \sim 1 \text{ W/cm}^2$ for 300W Hg, & a 6-inch diam. riser; also $P/A \sim 2000/[3.14 \cdot 30 \cdot 30/4] \sim 2.8 \text{ W/cm}^2$ for Xe & a 12-inch diam. riser

TABLE 2

Dwell Time for Compact/Short-arc Mercury & Xenon Lamps					
		Dose (J/l)			
Lamp type V	Wattage	50	100	200	500
Mercury 1W/cm ²	1	0.500	1.000	2.000	5.000
Xenon 2.5W/cm ²	2.5	0.200	0.400	0.800	2.000

Note that the dwell times are up to about a second if the irradiance is reduced by about a factor of 40, for example by reducing the lamp power to 10%, and increasing the cell diameter by x2 to 8" and 12" respectively. These are fairly large cells with low

1 power lamps, so it would take a lot of these to process very much water per day, making
2 their economic practicality more questionable.

3 For high power density processing cells, the dwell time is much shorter than the
4 between about 6-second to about 10-second dwell time indicated in the foregoing. In
5 order to get dwell times of between about 6 seconds to about 10 seconds, the lamp power
6 must be less than 10% of the kilowatt levels selected or predetermined, and the cell
7 diameters must be correspondingly much larger, e.g., up to 3x larger diameter. Those
8 numbers would not be very consistent with the geometry of the short/compact arc lamp
9 cylindrical risers; as such, the range of possible and feasible configurations for the system
10 according to the present invention is flexible to accommodate a variety of lamp types and
11 powers.

12 A main factor for consideration with respect to arc lamp spectra is the percentage
13 of UV light output found in approximately the disinfection wavelength region, namely
14 UVB&C from between about 200 to about 300 nm. The UV light sources contemplated
15 within the scope of the present invention indicate that the peak of the disinfection effect
16 occurs at about 265 nm. Also, the UV light available for disinfection effect is reduced
17 gradually on the short wavelength side, and rapidly on the long wavelength side.

18 Notably, low-pressure mercury (Hg) arc lamps are efficient radiators in the
19 UVB&C bands due to a resonant emission at about 254 nm. Advantageously, this is
20 close to the optimum UVC wavelength for disinfection of the fluid. Generally, the total
21 emission of radiation by a low-pressure tubular, germicidal lamp is about 20 to 35%,
22 depending on the design and operating parameters (the rest of the power being consumed
23 to heat the electrodes and the bulb) with 80 to 90% in about the 254 nm wavelength.

1 Thus, UVC efficacy is about 20 to 30%. The other principle line is at 365 nm, which is
2 outside the disinfection range. In some bulb designs it is the 365 nm line that dominates,
3 and the disinfection effect will be substantially reduced.

4 At low pressure, the plasma that forms the arc is in the "glow regime," which is
5 characterized by high electron temperatures, and much lower ion and neutral gas
6 temperatures (typically $T_e \sim 10,000\text{K}$, $T_i \sim T_g \sim 500\text{K}$). Under these conditions, the plasma
7 is optically transparent, and a few, very narrow emission "lines" characterize the
8 spectrum. Here, the emissivity will be low < 0.1 .

9 As the plasma temperature and density is increased (requiring higher current), the
10 arc temperature increases. The plasma becomes optically thick, and the electron, ion and
11 neutral gas temperature become comparable. The spectrum becomes characterized by a
12 blackbody continuum with a few lines superposed on it. A rule of quantum physics is
13 that the peak of the lines must be below the blackbody curve for that temperature, so a
14 blackbody curve can be fit to the peaks of the lines to deduce the effective arc
15 temperature, but the bulk of the emission will be from the continuum under the lines.

16 As an example, consider the high pressure Argon, commercially available Vortek
17 lamp. This lamp is a high pressure Argon arc operated at very high loading (P_{in}/L). To
18 be specific, consider the 100 kW lamp. The length is 20 cm, so the loading is 5 kW/cm.
19 The radiated output is given as 40 kW, 2 kW/cm so the efficiency is 40% (other Vortek
20 lamps are up to, and perhaps exceeding 50% radiative efficiency. The spectrum indicates
21 a peak at 800 nm which corresponds to an arc temperature deduced from Wien's law
22 $(2898\text{K}/W_{\max}(\mu\text{m})) = T(\text{K})$ of $\sim 3600\text{K}$ (the quoted figure is 3800K). Calculating the

1 blackbody emission from the arc with diameter 1.1 cm at 3800K, the result gives 1.8
2 kW/cm with emissivity of 0.4.

3 The UVB&C emission of the Vortek 100 kW lamp rises almost linearly from 200
4 to 300 nm. Thus, the UVB&C efficacy is about 5 %, and the UVB&C emission is about
5 5 kW. Notably, this is near the blackbody limit for a higher temperature (6500K). The
6 low emissivity occurs through the visible and NIR spectrum. Additionally, the lamps
7 emit about 5% UVB&C-200 to 300 nm, 10% UVA300-400 nm, 30% visible-400 to 700
8 nm, and 50% NIR at 700 to 1400 nm). However, the results are affected by arc
9 temperature; the results set forth herein are associated with low arc temperature. As the
10 arc temperature is increased, the amount of UVB&C increases dramatically, e.g., if the
11 arc temperature is increased to 8600K, the UVB&C efficacy increases to 20%, which is
12 comparable to the germicidal lamps.

13 Notably, the UV content in these lamps is much higher in comparison to that of
14 the Vortek lamp. Vortek estimate is T~ 3800K and about 1.5% in UVB&C, while the
15 lamp of figure 1b is T~8000K about 9% in UVB&C. Assuming an overall efficiency of
16 50%, the result is about 5% UVB&C efficiency.

17 The following analysis relates to a high-pressure xenon (Xe) lamp. For a 20 kW xenon
18 short arc, the peak blackbody emission is about 660 nm and corresponding to a
19 temperature of about 4500K. The spectrum is quasi-blackbody, with an estimated
20 emissivity of between about 60 to about 80%. The UVB&C emission of this lamp is
21 about 3% of the total but appears to have a glass cut off at about 240 nm; as such, the
22 emissivity may be higher, about 6%. For a total emission efficiency of 70%, the
23 corresponding UVB&C is between about 2% to about 4%.

1 The following analysis is associated with a high-pressure mercury (Hg) lamp,
2 wherein a short-arc lamp appears to be fairly low pressure as characterized by a line
3 spectrum. The spectrum representative of a high pressure Hg lamp notably includes a
4 predominant line at about 254 nm, which is in the well-established UVB&C disinfection
5 range. Most of the UV appears in the UVA range 300 to 400 nm, which is not useful
6 according to the prior art systems; surprisingly, this high-pressure lamp is effective when
7 used in the preferred embodiments according to the present invention. However, the
8 spectrum is more difficult to quantify than those of lamps set forth in the foregoing, with
9 an apparent temperature of about 8000K and an emissivity of approximately about 0.1.
10 Generally, the high pressure lamps will have lower UVB&C efficacy than the low
11 pressure germicidal lamps, but due to the higher power rating will have much more total
12 UVB&C emission.

13 Additionally, there exists a commercially available High Power Lamp (HPL) in
14 this long cylindrical form, made by Fusion Systems, and driven by a RF power source
15 (rather than DC as most of the rest) that also works effectively with the UV fluid
16 disinfection system and method according to the present invention. The discharge of this
17 HPL is electrodeless, and the lamp life is good, approximately 5000 hours. These tubular
18 lamps are most consistent with axial flow systems and retrofit design configurations for
19 embodiments of the present invention, or Planar Vertical Riser (PVR) systems. The
20 parameters for the Compact/Short-arc Lamps (CSL) and Cylindrical Vertical Riser
21 (CVR) are consistent with the calculations and examples set forth herein.

22 The fundamental physical parameters that control the design for these kinds of
23 systems are the lamp power per unit length, P/L, the dosing required, D =

1 Energy/volume, and the flow rate & dwell time. Considering the dwell time to be T =
 2 about 1 to about 100 seconds, the water penetration to be about 10 cm, which gives a
 3 flow velocity of about 1 cm/s for about 10 second dwell. The dwell time depends on the
 4 effectiveness of the turbulent mixing, effluent characteristics, and type of contamination.

5 The LPL, MPL, HPL, and UHPLs generally have the following characteristics:

TUBULAR LAMP CHARACTERISTICS				
Lamp type	Power	Length	Power/length	
8 LPL	<300W	~ 50cm	<3 W/cm	
9 MPL	300 to 3000W	~100cm	3 to 30W/cm	
10 HPL	2000 to 6000W	~ 25cm	240W/cm	
11 UHPL	50kW to 1000kW	~ 40cm	1 to 3kW/cm	

13 Nominal values are used for these calculations, realizing that the lamp power/length can
 14 be adjusted by the pressure, current (input power), and the like. Because of the large
 15 difference in power/length (P/L), these lamps are suitable to be used in very different
 16 geometries and are considered to be within the scope and contemplation of various
 17 embodiments constructed, set forth, and taught consistent with and according to the
 18 present invention.

19 Assuming a lamp length of between about 25 cm to about 100 cm, a range of
 20 practical sizes, (note that for tubular lamps the minimum is approximately about 15 cm
 21 with a maximum approximately about 150 cm). Furthermore, since the lamp arc
 22 diameter is in the range of between about 3 cm to about 6 cm, the flow cell width is sized
 23 to be about that wide or wider. Significantly smaller widths require impractical amounts
 24 of lamp transverse image demagnification, whereby demagnification in the longitudinal
 25 axis is probably impractical. Thus, practical cell cross-sectional areas are about at least a
 26 few hundred square centimeters, and the corresponding widths at least about 10 cm or

1 wider. At this point, it is assumed that the upper limit is to the flow cell width,
2 approximately a few meters.

3 The disinfection dosage, $D = \text{Energy/volume} = E/V$ varies from between about 50
4 J/liter to about 500 J/liter. The three parameters T , P/L , and D control the possible and/or
5 practical flow geometries according to the following equation:

6 $(P/L)/w/d = E/V/T = D/T$

7

8 Correspondingly, the flow channel width $[w]$ is set forth as follows:

9 $w = (P/L) * T / (D * d) = (P/L) * T / (D * d)$

10 $w = [P/L(W/cm) * T(sec)] / [D(J/l) * d(cm)] * [1000 \text{ cm}^3/\text{liter}]$

11

12 Analysis for the case for a 10-second water dwell (flow velocity ~ 1 cm/s) in the
13 irradiated volume follows.

14 For selected four lamp types and selected four water quality levels, the results are
15 approximately:

16

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TABLE 3
FLOW CELL WIDTH FOR VARIOUS TYPES OF WATER
10 SECOND DWELL
AND LAMPS TYPES
(cm)

Lamp type V	Dose (J/l)				
	50	100	200	500	1000
LPL 2W/cm	40	20	10	4	2
MPL 20 W/cm	400	200	100	40	20
HPL 200W/cm	4000	2000	1000	400	200
UHPL 2000W/cm	40000	20000	10000	4000	2000

For the LPL, the cell widths are reasonable, except perhaps for the highest dosage water. So a single LPL could be used for water treatment with a reasonable flow cell width as long as the water is reasonable pure. The LPL systems that have been deployed, the dosage is always under 100 J/l, so these lamps should be appropriate for small flow cells and low volumetric flow rates unless many of them are used. One way to get higher P/L for higher dosage water using LPLs is to use more lamps per cell. The use of a few lamps oriented in a half star pattern would allow these low P/L lamps to treat more water in a larger cell. Another way to use LPLs with the higher dosage water would be to reduce the flow velocity (increase the dwell time, see Table 3).

For the MPL the cell widths are larger, allowing higher volumetric flow rates. For example, a 200J/l system with a 20W/cm lamp would have a 2 kW lamp, and cell length and width of 100 cm. The MPL seems to be suitable for most water types at 10-

1 second dwell, except that the cells become a bit too large for the lowest dosage water. In
2 that case, the flow speed could be increased (decrease the dwell time, see Table 5)

3 The HPL (Fusion Lamp) has more than enough power to treat a system with a 10-
4 second dwell time, and is more suited to shorter dwell time processing (see Table 5).

5 The UHPL is not suitable with a planar vertical riser design with 10-second dwell, and
6 more suitable for a freely flowing configuration, or much shorter dwell times. Thus,
7 within some limits, both the LPL and MPL could be used with 10-second dwell for a
8 Planar Vertical Riser System, a preferred embodiment according to the present invention.

9 Where the dwell time is decreased to about 1 second, then the cross section could
10 be decreased by a factor of 10, and the flow velocity is correspondingly increased by the
11 same factor. Table 4 (below) shows these results for 1-second dwell (~10 cm/s flow
12 velocity):

TABLE 4

**FLOW CELL WIDTH FOR VARIOUS TYPES OF WATER
1 SECOND DWELL
AND LAMPS TYPES
(cm)**

Lamp type V	Dose (J/l)				
	50	100	200	500	1000
LPL 2W/cm	4	2	1	0.4	2
MPL 20 W/cm	40	20	10	4	20
HPL 200W/cm	400	200	100	40	200
UHPL 2000W/cm	4000	20000	1000	400	2000

17
18 The cell widths for LPL are too small, as is true for the MPLs width for the highest
19 dosage water. A MPL system is particularly effective for the lower dose water, and for

the higher dose water by using a few of the medium power lamps, and a somewhat wider cell. The HPL is now well suited to the flow channel size, except for the lowest dose water, where the dwell time would need to be reduced even further. The UHPL is appropriately used for large flow cells, provided that the dwell time is reduced respectively. For the highest dose water, the flow cells are of a practical size to work with a vertical riser system as shown in Figure 2, provided the light is allowed to diverge considerably, and subsecond dwell times are permissible, such as at the interface plate and associated UV dose zone.

As another illustration, consider the flow cell sizes for longer dwell water processing shown in Table 5.

TABLE 5
FLOW CELL WIDTH FOR VARIOUS TYPES OF WATER
100 SECOND DWELL
AND LAMPS TYPES
(cm)

Lamp type V	Dose (J/l)				
	50	100	200	500	1000
LPL 2W/cm	400	200	100	40	2
MPL 20 W/cm	4000	2000	1000	400	20
HPL 200W/cm	40000	20000	10000	4000	200
UHPL 2000W/cm	400000	200000	100000	40000	2000

With a 100 second dwell, the cell widths for all the higher power types of lamps are not necessarily the most practical design selection, although still functional

As the dwell time changes, the flexibility of system configuration according to the present invention permits that various tubular lamps can be used to process differing water types or fluids having various characteristics with reasonable flow cell cross-sections. The UHPLs can process all 4 water types (from between about 50 J/l to about 500 J/l) and at dwell time less than 1 second, as appropriate for a given fluid treatment system. HPLs can process water at dwell times around 1 second. MPLs can be used to process water with between about 1 to about 10-second dwell, with the longer dwell time being used for highest dosage and the shorter dwell time used for the lower dosage water. Additionally, LPLs are capable of processing the lower dosage water with about 10 second dwell and the higher dosage water with a 100 second dwell. A germicidal lamp system can be used for the longer dwell times, where the flow cell cross-section becomes small requiring different optical demagnification.

The following section sets forth selected particular design examples for particular water processing applications.

DESIGN EXAMPLES:

This section outlines a few design examples, not necessarily optimized, but illustrative of what can be done for a UV fluid disinfection system and method, wherein the fluid is water. These design examples include:

Laboratory effluent purifier

Home effluent purifier

Housing complex effluent purifier

Township effluent purifier

City effluent purifier

1 Large city effluent purifier

2 Megalopolis effluent purifier

3 **Laboratory effluent purifier (small mercury lamp)**

4 Mercury Lamp power < 150W, ~30,000 gallons per day (gpd). Flow cell is about
5 100 cm long by about 10 cm diameter.

6 The goal for this embodiment is to produce biologically disinfected water for
7 discharge into the municipal sewage system. The fluid is diluted to an acceptable level
8 by a turbidity dilution system. The UV dose required for disinfection of the water is low,
9 below about 100 J/l. One compact arc mercury lamp is used with a small cell,
10 approximately about 10 cm diameter by about 100 cm long with a maximum power of a
11 few hundred Watts. The water dwell time is about one second.

12 **Home effluent purifier (1 mercury lamp)**

13 Mercury Lamp power is less than about 150 W, approximately about 3000 gpd.
14 Flow cell is about 100 cm long by approximately about 10 cm diameter. In this case, it is
15 assumed that the effluent provided is previously treated sewage. It would be particularly
16 appropriate for homes that have independent water treatment facilities that discharge into
17 the local environment, such as coastal regions, remote locations, or resorts, or similar
18 localities. Assuming at least about 100 J/l are needed, but that less than 500 J/l will be
19 adequate for this type of system. The dwell time is about 100 seconds. The system is
20 designed to function on demand, capable of purifying effluent from a large household
21 using a small compact arc lamp, used in a configuration having a function similar to that
22 shown in Figure 5. Since a single lamp is used, a monitoring system or control system is

1 desirable to provide an indication when the lamp needs to be replaced or when other
2 service to the system is needed or suggested.

3 Since the water demand is relatively low and the cell water flow rate is relatively
4 high by comparison, the dwell could be increased whereby the lamp operates part of the
5 time or intermittently, either by sensing control or by timer. This intermittent-type
6 system arrangement beneficially extends the lamp life thereby providing a longer
7 replacement time or lamp life cycle. Since the lamp life is degraded by turning it off and
8 on, the system can be constructed and configured to allow the reservoir to be significantly
9 depleted before restarting the lamp (e.g., where a sewage reservoir or tank is used, the
10 lamp activity can be controlled, preprogrammed, and otherwise regulated to correspond
11 to the tank water size and water level. Depending on the size of the reservoir, and the
12 number of people using the system (as measured in discharged or used gallons/day), the
13 lamp is arranged, configured, and programmed to run intermittently, e.g., for an hour or
14 so per day. In this way, a lamp continuous operation life of about a month could be
15 extended to perhaps a year, depending upon the particular characteristics and
16 specifications of the system, including water characteristics.

17 **Housing complex effluent purifier (multiple mercury lamps)**

18 Mercury Lamp power approximately about 3 kW with approximately about
19 30,000 gpd. Six (6) Lamps at about 500 W, Flow cell about 100 cm long by about 20 cm
20 diameter. This design would be similar to the Home water purifier set forth in the
21 foregoing, except that it would use multiple lamps to accommodate the increased effluent
22 and use and to ensure operation in the event of a lamp failure. In this embodiment, the
23 lamps are constructed and controlled to run all of the time, and be replaced on a regular

1 maintenance schedule, e.g., weekly or monthly. If one lamp were to fail, that flow tube is
2 closed via an automatic lamp status detection system and control system. Approximate
3 dwell time associated with a typical configuration for this example is about a minute.

4 **Township water effluent purifier (dozens of mercury lamps)**

5 Mercury lamp power approximately about 12kW, including about a dozen 1 kW
6 lamps, approximately about 300,000 gpd. This system includes a small number of units
7 similar the previous housing complex unit, or a smaller number of larger units. This
8 system is capable of purifying the discharge water for a small town of a few thousand
9 people, using a few dozen small mercury lamps or a few higher power lamps, depending
10 upon system characteristics and specifications.

11 **City water effluent purifier (100's of Mercury lamps or perhaps a smaller number**
12 **of xenon lamps)**

13 Mercury lamp power approximately about 1MW, or Xenon lamp power
14 approximately about 1MW, about 10 Mgpd. This example could effectively be supported
15 by about 300 each of 3 kW lamps, and each cell being about 100 cm long. There are two
16 different approaches to the UV disinfectant system for this example: (1) to increase the
17 number of Mercury lamps as in the previous examples (it would take 100's of C/S HPLs),
18 or (2) to use less than about 1/3 as many Xenon lamps. Since the Xenon lamp is an
19 adequately efficient generator of UVB&C, it would simplify the construction and
20 maintenance of the system.

21 **Large City effluent purifier (thousand of Mercury, or perhaps a few hundred xenon**
22 **lamps)**

1 MPL lamp power approximately about 3MW, approximately about 30 Mgalpd.

2 This example is merely a scale-up of the previous water treatment systems. Clearly, the
3 advantage of the UHPLs is more apparent as scale increases.

4 **Megalopolis effluent purifier (few thousand Mercury lamps)**

5 MPL lamp power approximately about 10 MW, about 100+ Mgalpd. Continuing
6 the scale-up to a capacity for 1 million people. This is comparable to commercial
7 applications of the prior art larger Trojan Tech system, except that the present invention
8 advantageously uses much fewer, higher power Compact/Short arc Lamps, and in a non-
9 submerged configuration thereby providing more effective UV dosing with less
10 maintenance and increased efficiency and effectiveness of the overall system.

11 For cylindrical flow cell configurations and consideration of specific scales of
12 applications for water purification systems using the UV disinfection system and method
13 according to the present invention, several scenarios are presented as follows by way of
14 estimation and illustration of the distinction and differences between the present
15 invention and prior art; the figures are not intended to be self-limiting for practical
16 application precision, but are used to facilitate understanding of the present invention and
17 its preferred embodiments.

18 For laboratory effluent purifier use: 1 mercury C/S HPL. A practical design is
19 achieved using one <300W High Pressure Compact/Short-arc Lamp or a few smaller
20 lamps (C/S HPLs). The flow cell is about 100 cm long by less than about 2.5 cm
21 diameter, the dwell time between about 16 seconds to about 33 seconds. For a home
22 effluent purifier: 1mercury C/S HPL. A home effluent purifier based on one low power
23 <300WC/S HPL is feasible. A cell about 100 cm long by about 2.5 cm wide works well.

1 The dwell time is approximately less than 167 seconds. For a housing complex effluent
2 purifier: 6 C/S HPLs; a system with six 500W C/S HPL is capable of purifying effluent
3 for a condo or apartment complex. The flow cell is about the same size as the home
4 effluent purifier, but the use of a plurality of lamps and vertical risers increases the flow
5 volume, giving the system more demand capacity. For a township effluent purifier: about
6 a dozen MPLs and flow cells are required to ensure disinfection at reasonable flow rates.
7 In this type of case and scale, a system based six 2 kW C/S HPLs or a larger number of
8 smaller lamps is effective. For a standard city effluent purifier: hundreds of C/S HPL, or
9 a smaller number of Xenon lamps, are used with the system and method according to the
10 present invention. A system based on a hundred C/S HPLs or a smaller number of xenon
11 lamps works to provide efficient and effective fluid disinfection by UV dosage and
12 exposure. For a large city effluent purifier: approximately about 1000 C/S HPLs
13 (mercury). A system based on thousands of MPLs or a few dozen UHPLs also works
14 effectively. For a megalopolis effluent purifier: thousands of C/S HPLs are required.
15 Significantly, since for this scale of application, thousands of C/S HPLS are needed, the
16 benefits of using higher power lamps becomes even stronger, and particularly effective
17 using the configurations of the UV fluid disinfection system and method according to the
18 present invention.

19 The use of Compact/Short-arc High Pressure Lamps and Cylindrical Vertical
20 Risers creates a more complex system than using Medium Pressure Lamps and Planar
21 Vertical Risers, due to the need for more lamp power, which is due to lower UVB&C
22 efficacy, and more complex riser geometry. However, the use of higher power xenon
23 lamps, depending on their somewhat uncertain UVB&C efficacy, reduces the number of

1 lamps required, depending on the fluid characteristics and flow rates desired. Thus, the
2 UV disinfectant system according to the present invention provides efficient and effective
3 treatment of fluid, particularly water in wastewater treatment and other industrial
4 applications.

5 The present invention requires some pretreatment of the wastewater in cases of
6 wastewater with high turbidity prior to exposure to UV dose zones of the present
7 invention. Traditional means for reducing turbidity including, but not limited to,
8 filtration, dilution, reverse osmosis and chemical treatment may be advantageously
9 employed to increase the UV efficacy of the system according to the present invention.
10 However, certain aspects of the preferred embodiment allow it to more easily handle high
11 turbidity fluids than the prior art.

12 The interface plate may induce turbulence or cause fluid cascade with a non-
13 planar surface, stair-step surface, downwardly sloping surface, or other the like. The
14 induction of turbulence is particularly advantageous when the fluid is turbid. Turbidity,
15 which is the state of water when it is cloudy from having sediment stirred up, interferes
16 with the transmission of UV energy and decreases the disinfection efficiency of the UV
17 light disinfection system. Thus, turbulence, by inducing rotation in the particle, causes
18 all aspects of a particle to be exposed to the UV light. Additionally, the photocatalytic
19 properties of the system reduce turbidity by degrading the compounds or particles
20 responsible for the turbidity. Furthermore, the reflective aspects of the surfaces of the
21 system enhance the efficacy of the system when operated under turbid conditions because
22 the UV light can strike the various aspects of a particle with the need for the particle to be
23 rotating, thus overcoming the opacity of the particle. Another aspect that enhances

1 performance under turbid conditions is the high UV light intensity of the system. The
2 high UV light intensity can more easily compensate for fluctuations in turbidity than
3 lower-intensity systems. Thus, the preferred embodiment has several characteristics that
4 enhance its performance under turbid conditions.

5 In cases where the water has high iron or manganese content, is clouded and/or
6 has organic impurities, it is usually necessary to pre-treat the water before it enters the
7 UV disinfection stage because deposits on the quartz-encased submerged UV lamps,
8 which are immersed in the water to be treated, interfere with the UV light transmission,
9 thereby reducing the UV dose and rendering the system ineffective. Prior art typically
10 employs UV purification in conjunction with carbon filtration, reverse osmosis and with
11 certain chemicals to reduce fouling between cleanings of the quartz sleeves that surround
12 the UV lamps. Thus, another advantage of the preferred embodiment is that turbidity
13 reduction is not necessary for the system to perform adequately, and thus the system
14 eliminates the need for expensive pre-treatment of the fluid to reduce turbidity.

15 The contribution of the reflectance of internal surfaces to the efficacy of the
16 system can be capitalized upon by incorporating UV-reflective materials and reflection-
17 enhance design into the reservoir. These same surfaces can also be manufactured such
18 that they incorporate photocatalysts, as previously taught for the interface plate.
19 Moreover, additional surfaces to support photocatalyst may be added to the reservoir or
20 VRC system. Thus, an integrated design that incorporates UV-reflectant materials, UV-
21 reflectant design, photocatalysts, and additional photocatalyst surfaces will greatly
22 enhance the efficacy of the system.

1 Certain modifications and improvements will occur to those skilled in the art upon
2 a reading of the foregoing description. By way of example, various optical components
3 are used depending upon the particular UV light source or lamp selection for a given
4 system. Also, a plurality of UV light source systems, either planar horizontal or retrofit
5 configurations and/or cylindrical vertical riser configurations, may be combined and
6 arranged in series to increase the flow rates for which effective UV disinfection of the
7 fluid occurs. Moreover, a wide range of fluid applications are contemplated within the
8 scope of the present invention, including application of the UV fluid disinfectant system
9 and method to wastewater, commercial and industrial wastewater, agricultural sludge and
10 other waste and wastewater, biomedical and bodily fluids, fluid contaminants influents,
11 and effluents, and the like are contemplated applications for the present invention,
12 without substantial departure from the embodiments and teachings contained within this
13 specification. Additionally, surface treatment, including non-planar surfaces, for UV
14 disinfection of microorganisms thereon are contemplated applications properly
15 considered within the scope of the present invention. All modifications and
16 improvements have been deleted herein for the sake of conciseness and readability but
17 are properly within the scope of the following claims.

18

CLAIMS

We claim:

1. An ultraviolet disinfection (UV) system for treating waste-containing fluid, the system comprising at least one light source positioned within a housing and connected to a power source for producing a UV light output from the housing, the system including at least one optical component positioned between the at least one light source and the UV light output from the housing, thereby producing a focused, controllable UV light output that has at least one UV dose zone for providing effective sterilization of microorganisms within the fluid.

2. The UV system according to claim 1, wherein the at least one UV light source is one lamp.

3. The UV system according to claim 1, wherein the at least one UV light source is a UV lamp.

4. The UV system according to claim 3, wherein the at least one UV light source is a spectral calibration lamp.

5. The UV system according to claim 3, wherein the at least one UV light source is an electrodeless lamp.

6. The UV system according to claim 3, wherein the at least one UV light source is a mercury halide lamp.

7. The UV system according to claim 1, wherein the at least one UV light source is a light pump device.

8. The UV system according to claim 7, wherein the output from the at least one UV light source is distributed by fiber optic transmission lines.

1 9. The UV system according to claim 7 wherein the fiber optic transmission lines
2 having a first end connected to the housing output such that the UV light output from the
3 housing passes through the fiber optic transmission lines and exiting from a second end
4 such that the UV light output exiting the fiber optic transmission lines is projected into
5 the water.

6 10. The UV system according to claim 8, wherein the fiberoptic lines include
7 acrylic fibers.

8 11. The UV system according to claim 8, wherein the fiberoptic lines include
9 glass fibers.

10 12. The UV system according to claim 8, wherein the fiberoptic lines include
11 liquid core fibers.

12 13. The UV system according to claim 8, wherein the fiberoptic lines include
13 hollow core fibers.

14 14. The UV system according to claim 8, wherein the fiberoptic lines include
15 core-sheath fibers.

16 15. The UV system according to claim 8, wherein at least one fluid-containing
17 device is connected to the light pump device via fiberoptic transmission lines.

18 16. The UV system according to claim 1, further including a non-fouling lamp
19 housing thereby eliminating cleaning of the lamp housing to ensure consistent UV
20 disinfection of the fluid.

21 17. The UV system according to claim 1, wherein the light housing is affixed to a
22 reservoir and the UV light output disinfects a substantially non-flowing water supply
23 contained within the reservoir.

1 18. The UV system according to claim 17, wherein the system has a non-vertical
2 riser configuration.

3 19. The UV system according to claim 1, wherein the lamp housing is affixed to a
4 reservoir with flowing water contained therein.

5 20. The UV system according to claim 2, further including a vertical riser
6 configuration (VRC) wherein the water is moved at a predetermined rate toward the UV
7 light output thereby producing an increasing UV dose within the water as it approaches
8 the light output.

9 21. The UV system according to claim 20, wherein the interface zone further
10 includes at least one additive that influence characteristics of the fluid as the fluid passes
11 through the interface zone and over the surface zone.

12 22. The UV system according to claim 21, wherein the at least one additive is
13 selected from the group consisting of TiO₂, WO₂, ZnO, ZnS, SnO₂, and PtTiO₂ and the
14 like.

15 23. The UV system according to claim 20, wherein the vertical riser configuration
16 system is portable.

17 24. The UV system according to claim 20, wherein the vertical riser configuration
18 system is scalable to applications.

19 25. The UV system according to claim 20, wherein the system is adaptable to be
20 removably connected to a piping system for carrying water to an end user output, such
21 that a multiplicity of systems may be positioned to function at a corresponding
22 multiplicity of end user outputs to provide disinfected, purified water in many locations at
23 once.

1 26. The UV system according to claim 1, wherein the at least one optical
2 component is selected from the group consisting of reflectors, shutters, lenses, splitters,
3 focalizers, mirrors, rigid and flexible light guides, homogenizer, mixing rods, manifolds
4 and other couplers, filters, gratings, diffractors, color wheels and fiber optic transmission
5 lines.

6 27. The UV system according to claim 1, wherein at least one optical component
7 is an off-axis optical component.

8 28. The UV system according to claim 1, wherein at least one optical component
9 is a gradient component.

10 29. The UV system according to claim 1, wherein at least one optical component
11 is UV transmissive.

12 30. The UV system according to claim 1, wherein at least one optical component
13 is UV reflective.

14 31. The UV system according to claim 1 wherein the at least one optical
15 component includes fiber optic transmission lines having a first end connected to the
16 housing output such that the UV light output from the housing passes through the fiber
17 optic transmission lines and exiting from a second end such that the UV light output
18 exiting the fiber optic transmission lines is projected into the water.

19 32. The UV system according to claim 26, wherein the at least one optical
20 component is a lens for focusing light from the light source through an output point in the
21 housing and into the water for disinfection thereof.

22 33. The UV system according to claim 32, wherein the lens is a parabolic lens.

1 34. The UV system according to claim 1, wherein the at least one UV dose zone
2 includes a water-air interface dose zone and a variable intra-fluid dose zone.

3 35. The UV system according to claim 1, wherein the at least one UV light source
4 is positioned outside the water to be treated thereby providing effective sterilization of
5 microorganisms within the water.

6 36. An ultraviolet disinfection (UV) system for treating waste-containing fluid,
7 the system comprising at least one light source positioned outside the fluid to be treated
8 and positioned within a housing and connected to a power source for producing a UV
9 light output from the housing, the system including at least one optical component
10 positioned between the at least one light source and the UV light output from the housing,
11 thereby producing a focused, controllable UV light output that has at least one UV dose
12 zone for providing effective sterilization of microorganisms within the fluid.

13 37. The UV system according to claim 36, wherein the at least one UV light
14 source is a single UV lamp.

15 38. The UV system according to claim 36, wherein the at least one UV light
16 source is a spectral calibration lamp.

17 39. The UV system according to claim 36, wherein the at least one UV light
18 source is an electrodeless lamp.

19 40. The UV system according to claim 36, wherein the at least one UV light
20 source is a mercury halide lamp.

21 41. The UV system according to claim 36, wherein the at least one UV light
22 source is a light pump device.

1 42. The UV system according to claim 36, wherein the at least one UV light
2 source is a pulsed lamp device.

3 43. The UV system according to claim 36, further including a non-fouling lamp
4 housing thereby eliminating cleaning of the lamp housing to ensure consistent UV
5 disinfection of the fluid.

6 44. The UV system according to claim 36, wherein the light housing is affixed to
7 a reservoir and the UV light output disinfects a substantially non-flowing water supply
8 contained within the reservoir.

9 45. The UV system according to claim 44, wherein the system has a non-vertical
10 riser configuration.

11 46. The UV system according to claim 36, wherein the lamp housing is affixed to
12 a reservoir with flowing water contained therein.

13 47. The UV system according to claim 36, further including a vertical riser
14 configuration (VRC) wherein the water is moved at a predetermined rate toward the UV
15 light output thereby producing an increasing UV dose within the water as it approaches
16 the light output.

17 48. The UV system according to claim 36, wherein the interface zone further
18 includes at least one additive that influence characteristics of the fluid as the fluid passes
19 through the interface zone and over the surface zone.

20 49. The UV system according to claim 48, wherein the at least one additive is
21 selected from the group consisting of TiO₂, WO₂, ZnO, ZnS, SnO₂, and PtTiO₂ and the
22 like.

1 50. The UV system according to claim 47, wherein the vertical riser configuration
2 system is scalable to applications.

3 51. The UV system according to claim 46, wherein the system is adaptable to be
4 removably connected to a piping system for carrying water to an end user output, such
5 that a multiplicity of systems may be positioned to function at a corresponding
6 multiplicity of end user outputs to provide disinfected, purified water in many locations at
7 once.

8 52. The UV system according to claim 36, wherein the at least one optical
9 component is selected from the group consisting of reflectors, shutters, lenses, splitters,
10 focalizers, mirrors, rigid and flexible light guides, homogenizer, mixing rods, manifolds
11 and other couplers, filters, gratings, diffractors, color wheels and fiber optic transmission
12 lines.

13 53. The UV system according to claim 36, wherein at least one optical component
14 is UV transmissive.

15 54. The UV system according to claim 36, wherein at least one optical component
16 is UV reflective.

17 55. The UV system according to claim 36, wherein the at least one optical
18 component includes fiber optic transmission lines having a first end connected to the
19 housing output such that the UV light output from the housing passes through the fiber
20 optic transmission lines and exiting from a second end such that the UV light output
21 exiting the fiber optic transmission lines is projected into the water.

22 56. The UV system according to claim 55, wherein the fiberoptic lines include
23 acrylic fibers.

5 59. The UV system according to claim 55, wherein the fiberoptic lines include
6 hollow core fibers.

9 61. The UV system according to claim 52, wherein the at least one optical
10 component is a lens for focusing light from the light source through an output point in the
11 housing and into the water for disinfection thereof.

63. The UV system according to claim 36, wherein the at least one UV dose zone
includes a water-air interface dose zone and a variable intra-fluid dose zone.

16 providing the fluid to be treated in a reservoir;

producing a focused, controllable UV light output that has at least one UV dose
zone for providing effective sterilization of microorganisms within the water.

1 65. The method according to claim 64, wherein the system includes a non-
2 submerged light source.

3 66. A method for providing ultraviolet disinfection (UV) of waste-containing
4 fluids, the method comprising the steps of

5 providing a UV disinfection system comprising at least one UV light
6 source coupled with at least one UV-transmissive optical component outside a fluid to be
7 treated and at least one interface zone positioned between the at least one UV light source
8 and the fluid to be treated, the at least one UV light source designed, configured, and
9 connected to produce UV light creating at least one UV dose zone outside the fluid;

10 presenting a surface zone on the at least one interface zone, wherein the surface
11 zone has a UV dose zone associated therewith for disinfecting the fluid to be treated;

12 introducing a pre-treated fluid into the system, the fluid passing through at least
13 one UV dose zone within the fluid and passing through the at least one interface zone and
14 surface zone UV dose zone;

15 disinfecting the fluid via exposure to the UV light in the UV dose zones;

16 dispensing the disinfected fluid outside the system.

17 67. The method according to claim 66, further including the step of forcing
18 water via a hydraulic system through a vertical riser configuration of the system.

19 68. The method according to claim 66, further including the step of modifying
20 the fluid characteristics via at least one additive on the interface zone causing a reaction
21 in the fluid.

1 69. The method according to claim 66, further including the step of
2 introducing turbulence in the fluid as the fluid passes throughout the system, thereby
3 increasing the exposure to UV light, disinfection, and catalytic chemical reactions.

4 70. The method according to claim 66, further including the step of
5 introducing a catalyst at the interface zone.

6

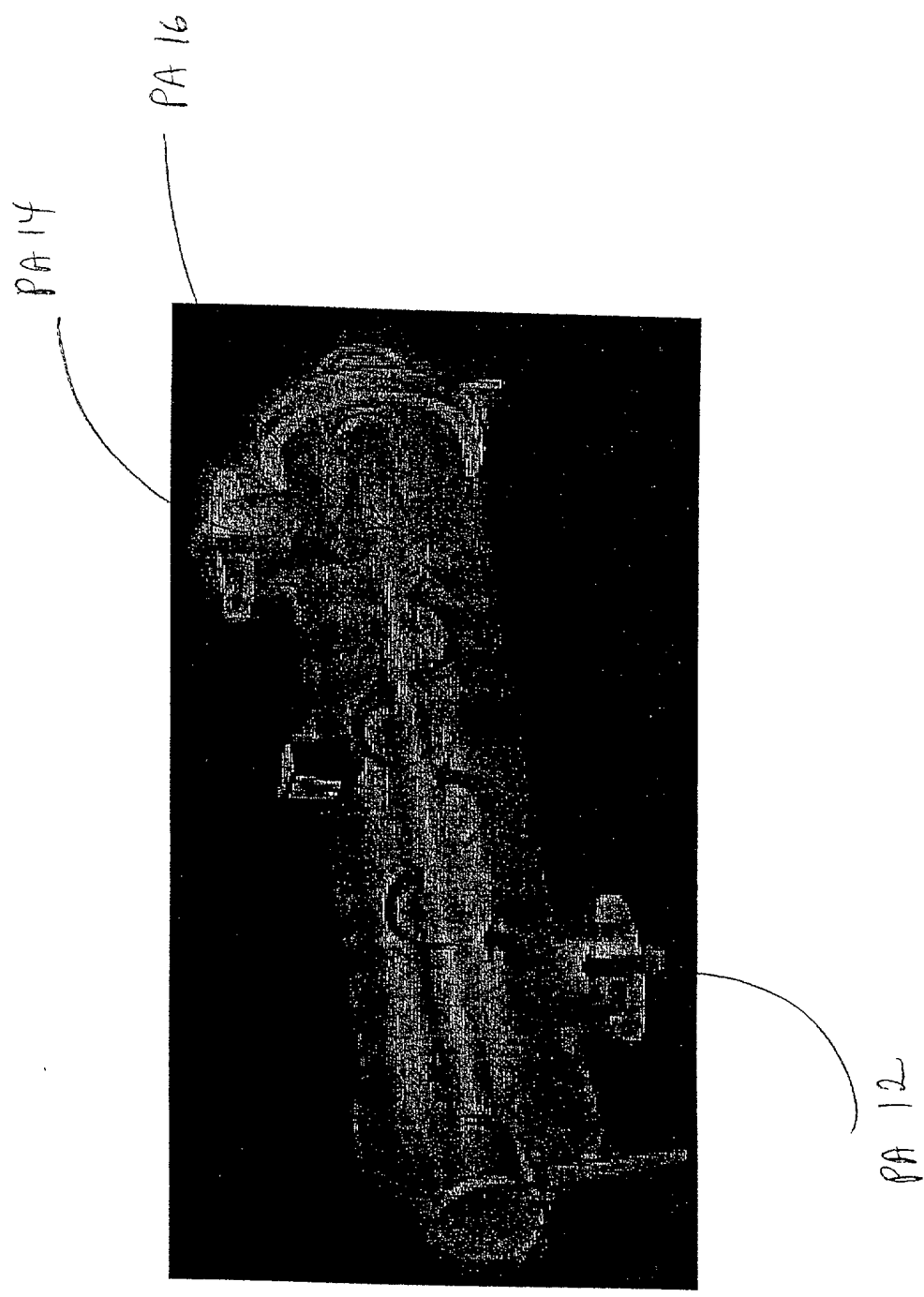
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ABSTRACT

An ultraviolet (UV) disinfection system and method for treating for treating waste-containing fluids including a configuration and design to function effectively with at least one UV light source or lamp that is not submerged in the fluid. The UV light source is positioned outside the fluid to be disinfected via exposure to at least one UV dose zone outside the fluid being treated wherein UV light is projected into the at least one dose zone. The UV light source may be presented in a vertical riser configuration, wherein the UV light source is positioned above the fluid to be treated and projecting a UV dose zone downward toward and into the fluid to be treated, with the fluid moving upward toward the UV light source. At least one interface plate is used to provide a surface zone for UV disinfection above the fluid and to provide additional treatment means for balancing pH, affecting effluent chemistry, reducing organic chemicals, and the like. Alternatively, the UV light source may be presented in a planar or horizontal design, wherein the UV light source is positioned above the fluid to be treated and projecting a UV dose zone downward toward and into the fluid to be treated, with the fluid moving in a direction substantially perpendicular to the UV dose zone. Thirdly, the UV light source may be presented in a reservoir configuration, wherein the UV light source is positioned above the fluid to be treated that is contained in a reservoir.

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Figure 1: Prior Art



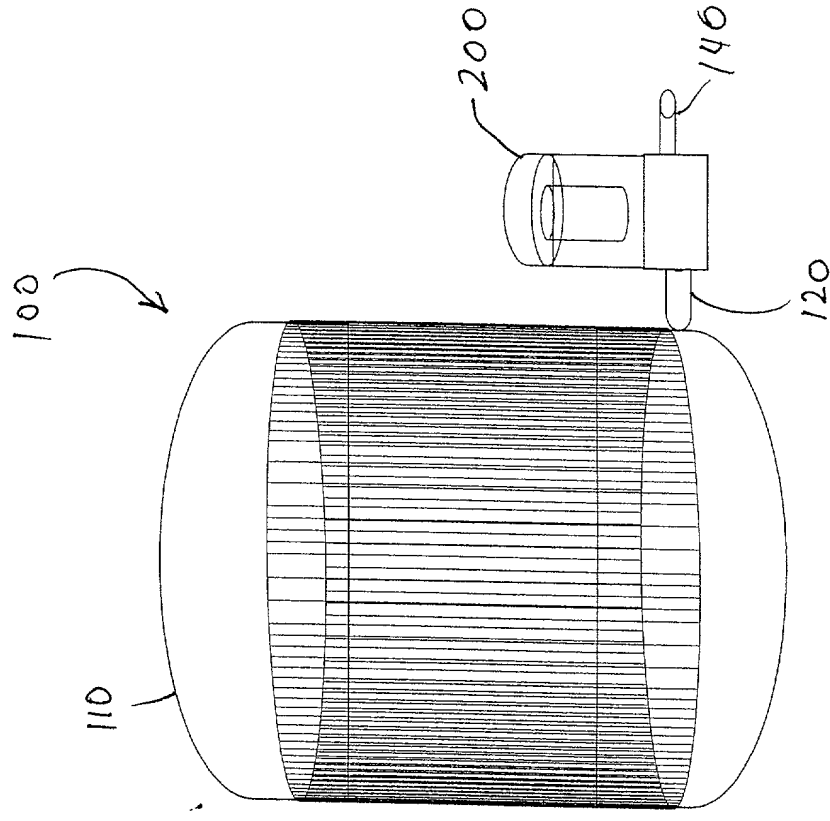
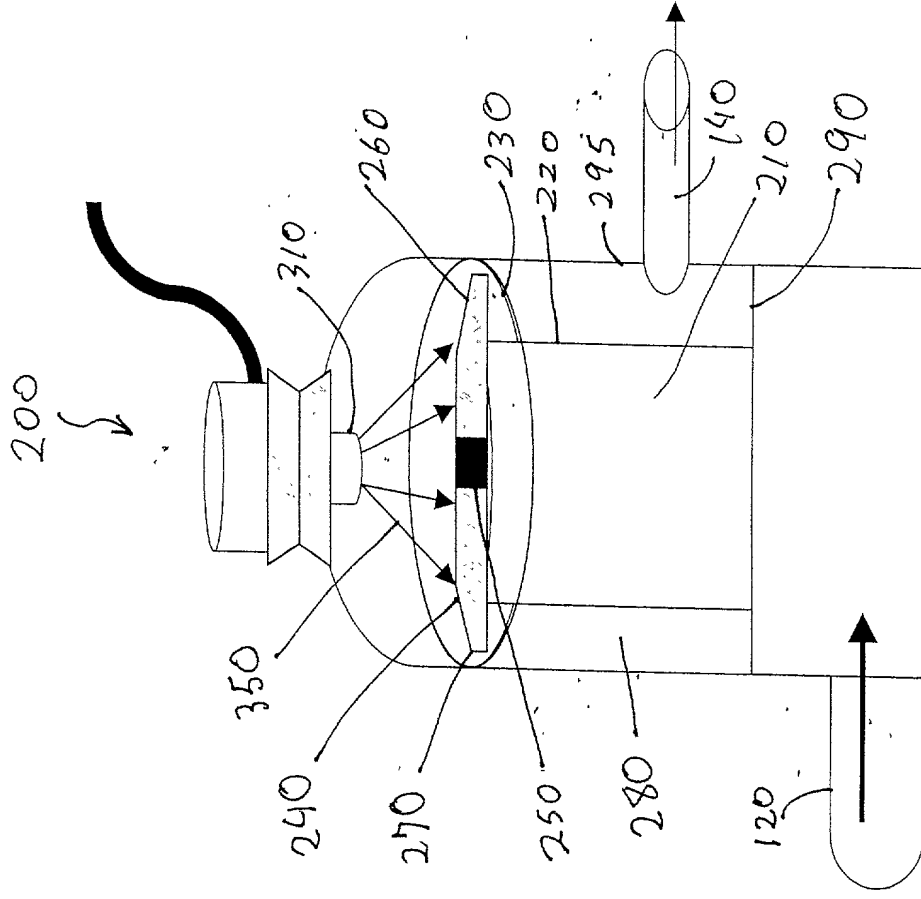
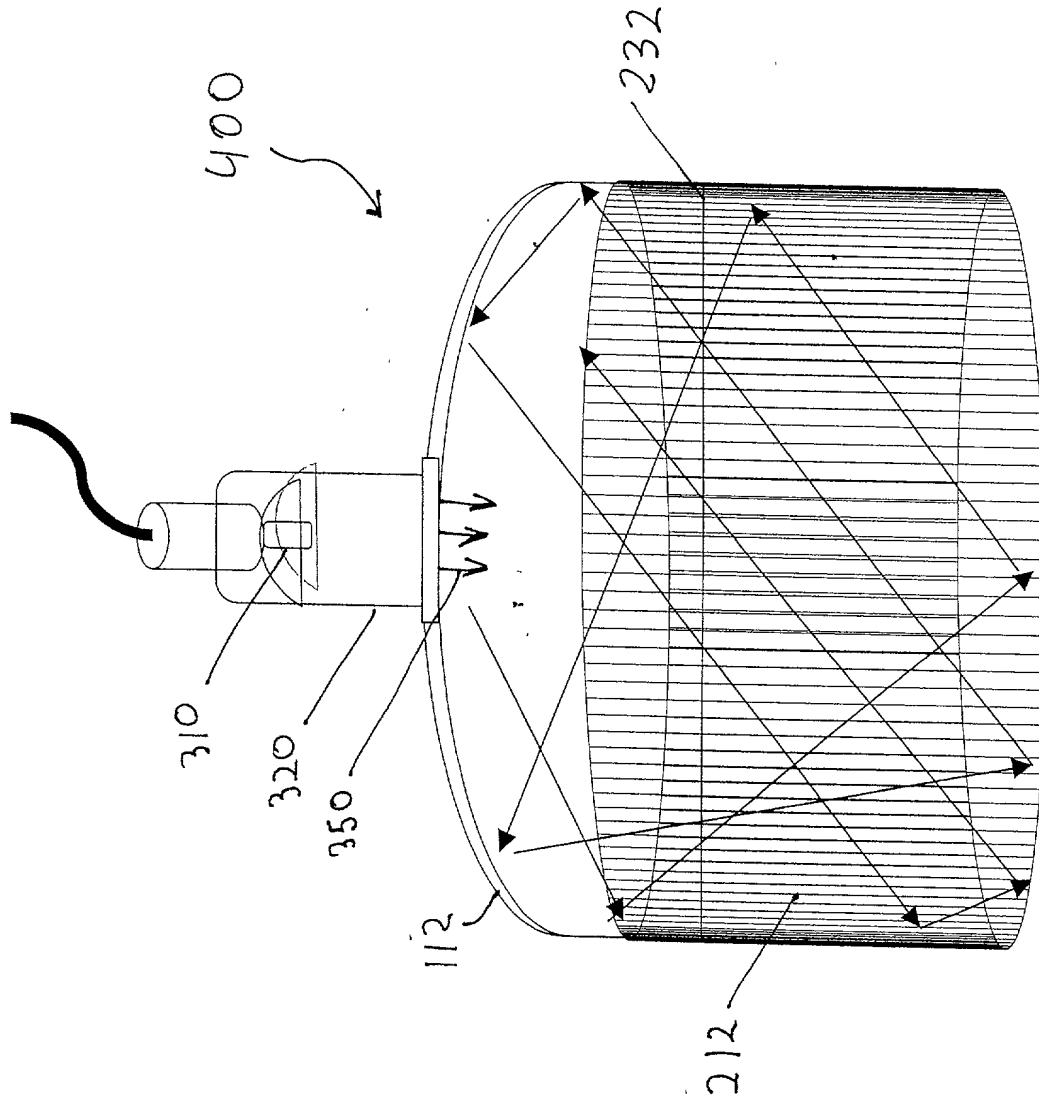
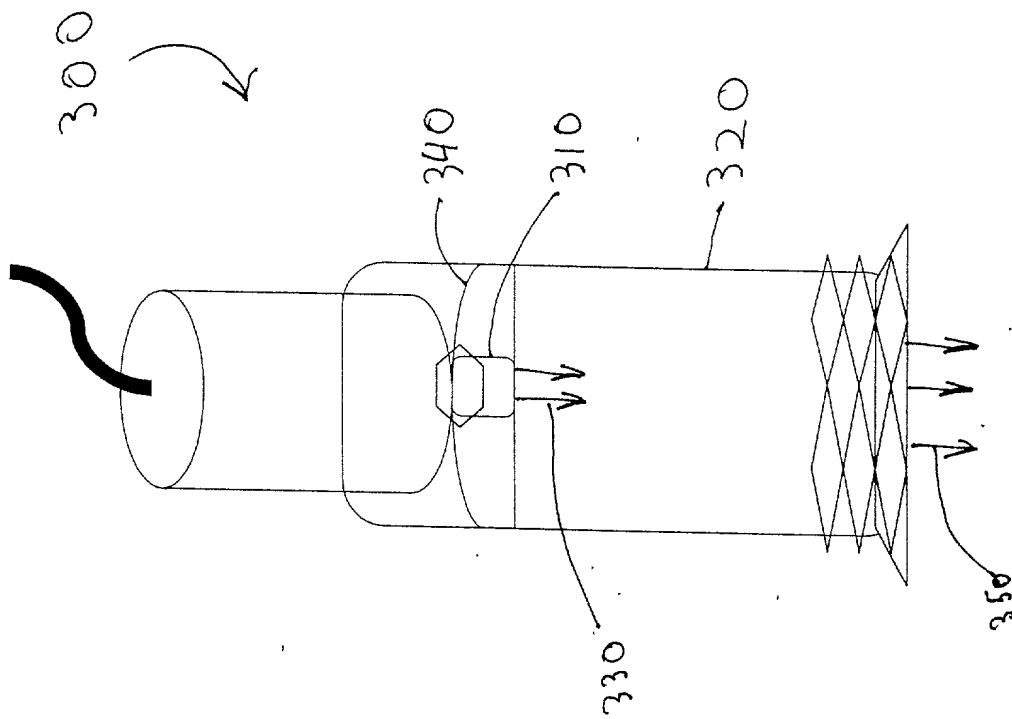


FIG. 2







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Fig. 5

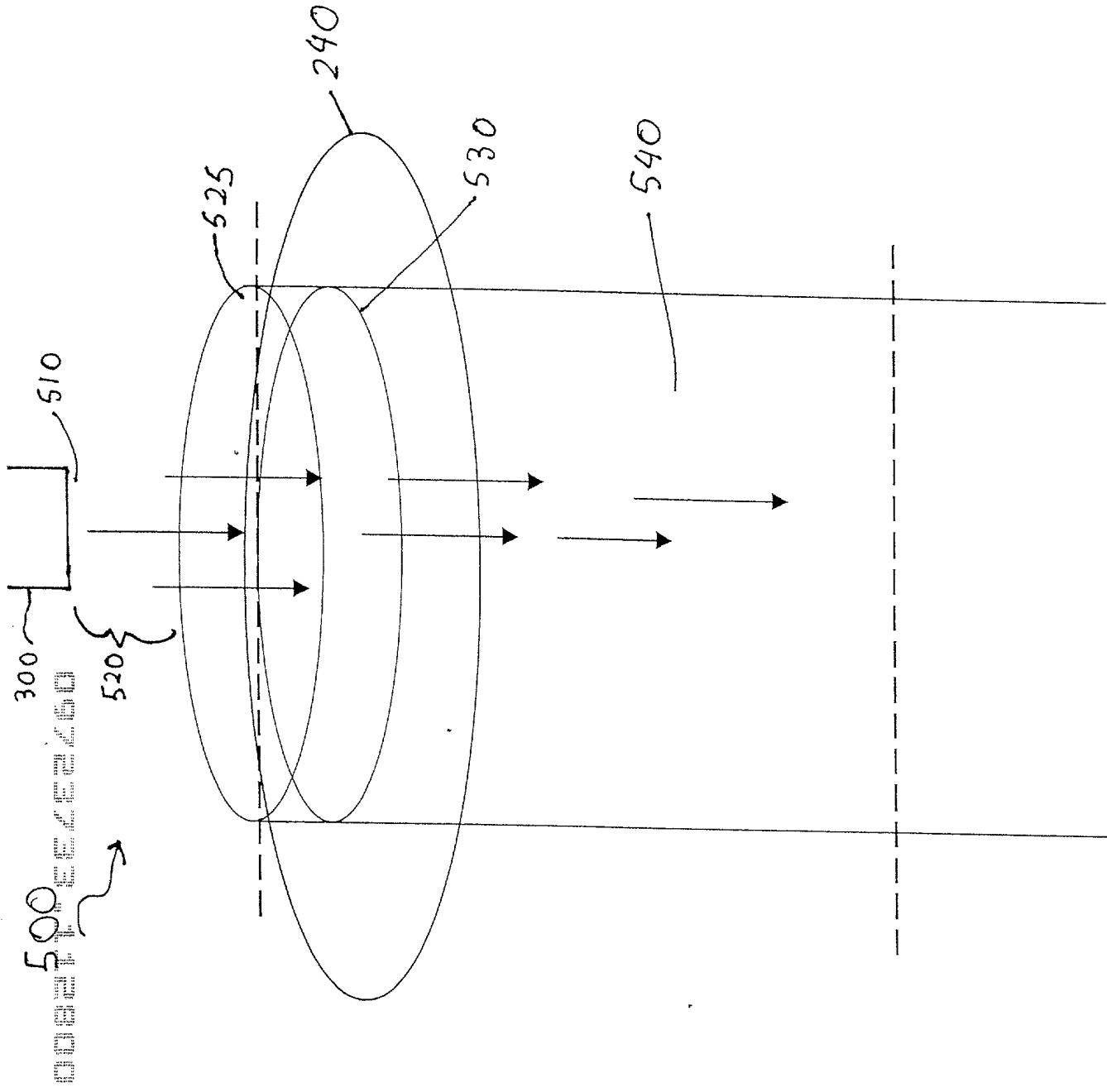


Figure 6

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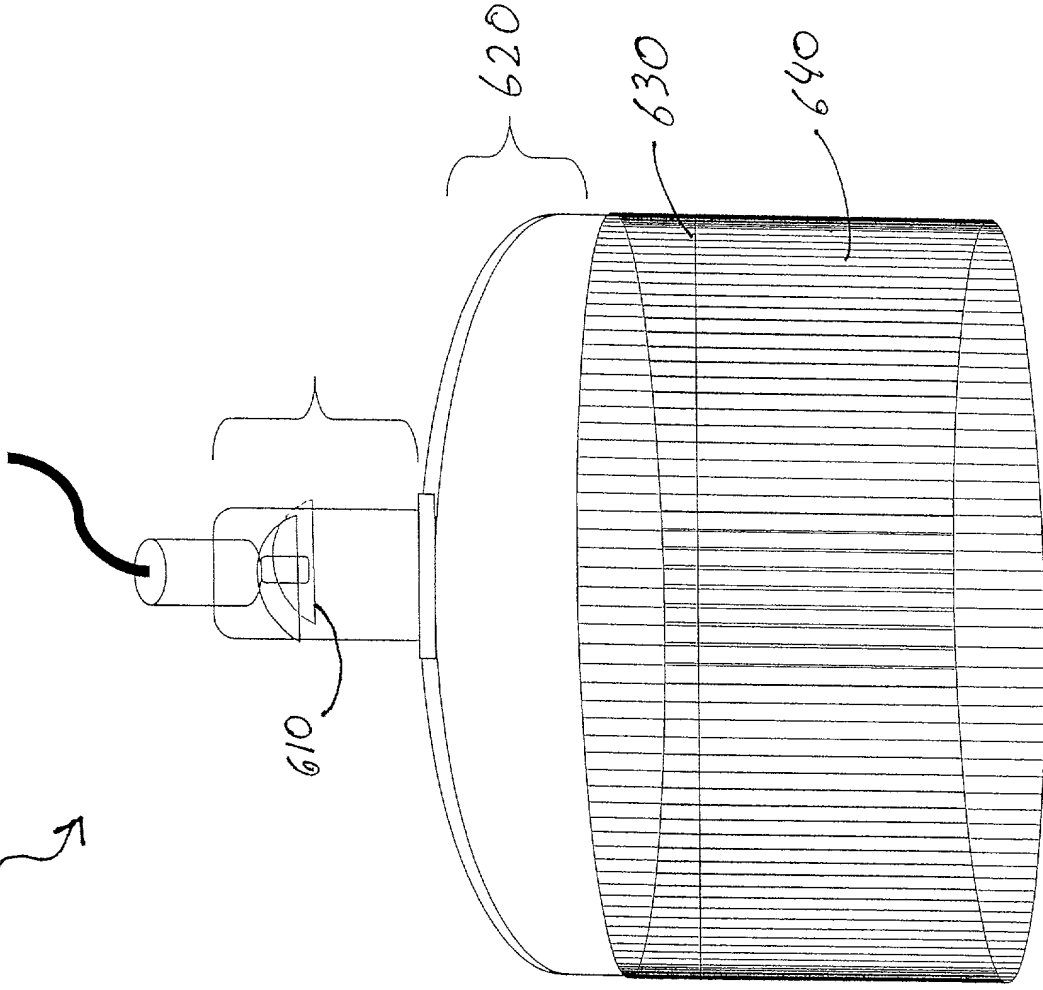


Figure 7

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PATENT APPLICATION
(37 CFR 1.63)**

☒ Declaration Submitted with Initial Filing **OR** ☐ Declaration Submitted after Initial Filing (surcharge (37 CFR 1.16 (e)) required)

Attorney Docket Number 1300-009

First Named Inventor Horton

COMPLETE IF KNOWN

Application Number

Filing Date

11/28/2000

Group Art Unit

Examiner Name

As a below named inventor, I hereby declare that:

My residence, post office address, and citizenship are as stated below next to my name.

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled:

UV DISINFECTION OF WASTEWATER DEVICE AND METHOD

the specification of which

(Title of the Invention)

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[Page 1 of 2]

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U.S. Parent Application or PCT Parent Number	Parent Filing Date (MM/DD/YYYY)	Parent Patent Number (if applicable)
09/630 245	07/31/2000	

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OR

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Name	Registration Number	Name	Registration Number
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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under 18 U.S.C. 1001 and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

Name of Sole or First Inventor:

☐ A petition has been filed for this unsigned inventor

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City	State	ZIP	Country
Raleigh	NC	27615	USA

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